# A non-iterative method for computing the infimum in $H_{\infty}$ -optimization

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This paper presents a simple and non-iterative procedure for the computation of the exact value of the infimum in the singular  $H_{\infty}$ -optimization problem, and is an extension of our earlier work. The problem formulation is general and does not place any restriction on the direct feedthrough terms between the control input and the controlled output variables, and between the disturbance input and the measurement output variables. Our method is applicable to a class of singular  $H_{\infty}$ -optimization problems for which the transfer functions from the control input to the controlled output and from the disturbance input to the measurement output have no invariant zeros on the  $j\omega$  axis and also satisfy certain geometric conditions. The computation of the infimum in our method involves solving two well-defined Riccati and two Lyapunov equations.

## **Conventions and notation**

- $A^{\mathrm{T}}$  transpose of A
  - I identity matrix
  - $\mathbb{R}$  set of real numbers
  - C whole complex plane
- $\mathbb{C}^-$  open left-half complex plane
- $\mathbb{C}^+$  open right-half complex plane
- $\mathbb{C}^0$  imaginary axis j $\omega$
- $\sigma_{\max}(A)$  maximum singular value of A
  - $\lambda(A)$  set of eigenvalues of A
- $\lambda_{\max}(A)$  maximum eigenvalue of A where  $\lambda(A) \subset \mathbb{R}$ 
  - $\rho(A)$  spectral radius of A
- Ker(V) kernel of V
- Im(V) image of V

#### 1. Introduction

The past decade has witnessed a proliferation of literature on  $H_{\infty}$ -optimal control since it was first introduced by Zames (1981). The main focus of the work has been, and continues to be, on the formulation of the problem for robust multivariable control and its solution. Since the original formulation of the  $H_{\infty}$ -problem in Zames (1981), a great deal of the work has been on the solution to this problem. Practically all research results of early years involved a mixture of time-domain and frequency-domain techniques (Doyle 1984, Francis

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1987, Glover 1984). Recently, considerable attention has been focused on purely time-domain methods based on algebraic Riccati equations (ARE) (Doyle et al. 1989, Doyle and Glover 1988, Khargonekar et al. 1988, Petersen 1987, 1988; Sampei et al. 1990, Stoorvogel 1991, Stoorvogel and Trentelman 1990, Zhou and Khargonekar 1988). Along this line of research, connections are also made between  $H_{\infty}$ -optimal control and differential games (Basar and Bernard 1989, Papavassilopoulos and Safonov 1989). Typically in ARE approaches to  $H_{\infty}$ -optimal control problems, the achieved design solution is suboptimal in the sense that the  $H_{\infty}$ -norm of the closed-loop system transfer function from the disturbances to the controlled outputs is less than a prescribed value. For the regular case, (this refers to a system where the feedthrough matrix from the disturbance to the measurement output is surjective and the feedthrough matrix from the control input to the controlled output is injective) the existence of suboptimal state (output) feedback laws is formulated in terms of the existence of a stabilizing positive semi-definite solution(s) for one (two) 'indefinite' algebraic Riccati equation(s) and the satisfaction of a coupling condition for the case of output feedback. A recent paper by Stoorvogel (1991) has shown that conditions for the existence of suboptimal output feedback laws for the general singular case (i.e. not a regular case) can be expressed in terms of the existence of solutions to two quadratic matrix inequalities. Solutions of these inequalities must also satisfy two rank conditions and a coupling condition. The latter condition requires that the spectral radius of the product of the two solutions to be smaller than a certain prior given upper bound.

In this paper, we address the problem of computing the infimum in  $H_{\infty}$ -optimization for the output feedback case. The ARE-based approach to this problem simply provides an iterative scheme of approximating the infimum (denoted here by  $\gamma_0^*$ ) of the  $H_{\infty}$ -norm of the closed-loop transfer function using output feedback compensators. For example, in the regular case and utilizing the results of Doyle et al. (1989), an iterative procedure for approximating  $\gamma_0^*$ would proceed as follows: one starts with a value of  $\gamma$  and determines whether  $\gamma > \gamma_0^*$  by solving two 'indefinite' algebraic Riccati equations and checking the positive semi-definiteness and stabilizing properties of these solutions. In the case where such positive semi-definite solutions exist and satisfy a coupling condition, then we have  $\gamma > \gamma_0^*$  and one simply repeats the above steps using a smaller value of  $\gamma$ . In principle, one can approximate the infimum  $\gamma_0^*$  to within any degree of accuracy in this manner. However this search procedure is exhaustive and can be very costly. More significantly, due to the possible high-gain occurrence as  $\gamma$  gets close to  $\gamma_0^*$ , numerical solutions for these AREs can become highly sensitive and ill-conditioned. This difficulty also arises in the coupling condition. Namely, as  $\gamma$  decreases, evaluation of the coupling condition would generally involve finding eigenvalues of stiff matrices. These numerical difficulties are likely to be more severe for problems associated with the singular case. So, in general, the iterative procedure for the computation of  $\gamma_0^*$  based on AREs is not reliable and thus should not be used to determine the infimum  $\gamma_0^*$ .

In a recent paper of Chen *et al.* (1992), a non-iterative algorithm was proposed to calculate  $\gamma_0^*$  for a class of systems that satisfy the following conditions: (i) the transfer function from the control input to the controlled output is right-invertible and has no invariant zeros on the j $\omega$  axis; and (ii) the transfer function from the disturbance to the measurement output is

left-invertible and has no invariant zeros on the j $\omega$  axis. The goal of this paper is to generalize and extend the results of Chen *et al.* (1992) by relaxing the above assumptions; namely, to replace the right- and left-invertibility assumptions imposed on the given plant by two geometric conditions, which are much weaker than the former ones. We would like to point out that under the assumptions of Chen *et al.* (1992), the computation of  $\gamma_0^*$  involves solving four Lyapunov equations. However, the computation of  $\gamma_0^*$  under the new assumptions of this paper requires solving two well-defined Riccati and two Lyapunov equations. The new algorithm has been implemented efficiently in a MATLAB-software environment for numerical solutions.

The outline of this paper is as follows. In §2 we introduce the problem statement. In §3 we provide some preliminaries on the special coordinate basis (s.c.b) and its properties for non-strictly proper systems, and the main results of Stoorvogel (1991) in notations consistent with the problem statement of §2. The s.c.b transformation and Stoorvogel's theorem are both instrumental in the derivation of the main results given in §4 for the exact computation of  $\gamma_0^*$ . Section 5 gives other related results on problems of almost disturbance decoupling with internal stability, and conditions under which the infimum of the output feedback case is equal to that of the state feedback case. Finally in §6 we draw the conclusion.

We refer to the linear dynamical system

$$\dot{x} = Ax + Bu, \quad y = Cx + Du \tag{0.1}$$

as the system (A, B, C, D). We also refer to  $T_{yu}(s) = C(sI - A)^{-1}B + D$  as the transfer function matrix of the system (A, B, C, D) between the input u and the output y. For any real rational matrix T(s),

$$||T||_{\infty} := \sup \left\{ \sigma_{\max}[T(j\omega)] : \omega \in \mathbb{R} \right\}$$
(0.2)

then  $||T||_{\infty}$  coincides with the  $L_{\infty}$ -norm of T(s) if T(s) is proper and has no poles in  $\mathbb{C}^0$ , and with the  $H_{\infty}$ -norm of T(s) if it is proper and stable. We also define the following subspaces:

- (i)  $\mathcal{V}^{g}(A, B, C, D)$ —the maximal subspace of  $\mathbb{R}^{n}$  which is (A + BF)-invariant and contained in Ker(C + DF) such that the eigenvalues of  $(A + BF)|\mathcal{V}^{g}$  are contained in  $\mathbb{C}_{g} \subseteq \mathbb{C}$  for some F.
- (ii)  $\mathcal{S}^{g}(A, B, C, D)$ —the minimal (A + KC)-invariant subspace of  $\mathbb{R}^{n}$  containing Im (B + KD) such that the eigenvalues of the map which is induced by (A + KC) on the factor space  $\mathbb{R}^{n}/\mathcal{S}^{g}$  are contained in  $\mathbb{C}_{g} \subseteq \mathbb{C}$  for some K.

For the cases that  $\mathbb{C}_g := \mathbb{C}$ ,  $\mathbb{C}_g = \mathbb{C}^-$  and  $\mathbb{C}_g = \mathbb{C}^0 \cup \mathbb{C}^+$ , we replace the index g in  $\mathcal{V}^g$  and  $\mathcal{S}^g$  by '\*', '-' and '+' respectively.

# 2. Problem formulation

Let us consider the following linear system,

$$\sum : \begin{cases} \dot{x} = Ax + Bu + Ew \\ y = C_1 x + D_1 w \\ z = C_2 x + D_2 u \end{cases}$$
(2.1)

where  $x \in \mathbb{R}^n$  is the state,  $u \in \mathbb{R}^m$  is the input,  $w \in \mathbb{R}^p$  is the disturbance,  $y \in \mathbb{R}^r$  is the measured output available for feedback control and  $z \in \mathbb{R}^q$  is the controlled output. Let  $T_{zw}(s)$  denote the closed-loop transfer function matrix from the disturbance w to the controlled output z. The standard  $H_{\infty}$ -optimal control problem is concerned with the construction of stabilizing feedback control-laws that minimize the  $H_{\infty}$ -norm of  $T_{zw}(s)$ . We consider three different classes of control laws: static-state feedback, dynamic-state feedback and dynamic-output feedback laws. Furthermore, we denote the infimum of the  $H_{\infty}$ -norm achieved under these three classes of feedback laws as  $\gamma_s^*$ ,  $\gamma_d^*$  and  $\gamma_0^*$ respectively. Namely,

- $\gamma_s^* := \inf \{ \|T_{zw}\|_{\infty} \text{ where } u(s) = Fx(s) \text{ for any } F \text{ which internally stabilizes the system of (2.1), i.e. } A + BF \text{ is a stability matrix} \}$
- $\gamma_d^* := \inf \{ \|T_{zw}\|_{\infty} \text{ where } u(s) = F_s(s)x(s) \text{ for any proper transfer function}$ matrix  $F_s(s)$  which internally stabilizes the system of (2.1)}
- $\gamma_0^* := \inf \{ \|T_{zw}\|_{\infty} \text{ where } u(s) = F_0(s)y(s) \text{ for any proper transfer function}$ matrix  $F_0(s)$  which internally stabilizes the system of (2.1)}

Zhou and Khargonekar (1988) have shown that  $\gamma_d^* = \gamma_s^*$  which also implies that  $\gamma_s^* \leq \gamma_0^*$ . It is also well-known that, in general,  $\gamma_0^*$  is not equal to  $\gamma_s^*$ . In this paper we give a simple and non-iterative procedure for determining  $\gamma_0^*$ . The method is applicable to the general system of (2.1) satisfying the following assumptions.

- (A1) The system  $(A, B, C_2, D_2)$  is stabilizable and has no invariant zeros in  $\mathbb{C}^0$ .
- (A2) Im  $(E) \subseteq \mathcal{V}^-(A, B, C_2, D_2) \cup \mathcal{G}^-(A, B, C_2, D_2).$
- (B1) The system  $(A, E, C_1, D_1)$  is detectable and has no invariant zeros in  $\mathbb{C}^0$ .
- (B2) Ker  $(C_2) \supseteq \mathcal{V}^-(A, E, C_1, D_1) \cap \mathcal{G}^-(A, E, C_1, D_1).$

Here we would like to note that the above (A1) and (B1) are the standard assumptions on  $H_{\infty}$ -optimization literature. On the other hand, (A2) and (B2) generalize the results of Chen *et al.* (1992), in which the subsystems  $(A, B, C_2, D_2)$  and  $(A, E, C_1, D_1)$  are required to be right- and left-invertible, respectively. In fact, if  $(A, B, C_2, D_2)$  and  $(A, E, C_1, D_1)$  are automatically satisfied.

One of the key components of our method is to put the problem in a special coordinate basis (s.c.b) introduced in Sannuti and Saberi (1987) and Saberi and Sannuti (1990) which explicitly exhibits the finite and infinite zero structures of the system. The other component utilizes the results of Stoorvogel (1991).

#### 3. Preliminaries

In the following section we shall recall the definition of the special coordinate basis (s.c.b) for a linear time-invariant non-strictly proper system (Saberi and Sannuti 1990), and the theorem of Stoorvogel (1991). Such a coordinate basis has a distinct feature of explicitly displaying the finite and infinite zero structures of a given system as well as other system geometric properties. The results of Stoorvogel provide conditions for the existence of an

 $H_{\infty}$ -norm bound solution in the output feedback case. They are both instrumental in the derivation of the method described in § 4.

#### 3.1. Special coordinate basis

In the following we recapitulate the main results in a theorem and some properties of the special coordinate basis while leaving detailed derivation and proofs to be found in Sannuti and Saberi (1987) and Saberi and Sannuti (1990). Consider the system described by

$$\begin{aligned} \dot{x} &= Ax + Bu \\ z &= Cx + Du \end{aligned}$$
 (3.1)

It can be easily shown that using singular value decomposition one can always find an orthogonal transformation U and a non-singular matrix V that put the direct feedthrough matrix D into the following form

$$\overline{D} = UDV = \begin{bmatrix} I_r & 0\\ 0 & 0 \end{bmatrix}$$
(3.2)

where r is the rank of D. Without loss of generality one can assume that the matrix D in (3.1) has the form as shown in (3.2). Thus, the system in (3.1) can be rewritten as

$$\dot{x} = Ax + \begin{bmatrix} B_0 & B_1 \end{bmatrix} \begin{pmatrix} u_0 \\ u_1 \end{pmatrix} \\ \begin{pmatrix} z_0 \\ z_1 \end{pmatrix} = \begin{bmatrix} C_0 \\ C_1 \end{bmatrix} x + \begin{bmatrix} I_r & 0 \\ 0 & 0 \end{bmatrix} \begin{pmatrix} u_0 \\ u_1 \end{pmatrix}$$
(3.3)

where  $B_0$ ,  $B_1$ ,  $C_0$  and  $C_1$  are the matrices of appropriate dimensions. Note that the inputs  $u_0$  and  $u_1$ , and the outputs  $z_0$  and  $z_1$  are those of the transformed system. Namely,

$$u = V \begin{pmatrix} u_0 \\ u_1 \end{pmatrix}$$
 and  $\begin{pmatrix} z_0 \\ z_1 \end{pmatrix} = Uz$ 

Note that the  $H_{\infty}$ -norm of the system transfer function  $T_{zw}(s)$  is unchanged when we apply an orthogonal transformation on the output z, and also under any non-singular transformations on the states and control inputs. We have the following main theorem.

**Theorem 3.1:** There exist non-singular transformations  $\Gamma_s$ ,  $\Gamma_0$  and  $\Gamma_i$  such that

$$\begin{aligned} x &= \Gamma_s[(x_a^+)^{\mathrm{T}}, x_b^{\mathrm{T}}, (x_a^-)^{\mathrm{T}}, x_c^{\mathrm{T}}, x_f^{\mathrm{T}}]^{\mathrm{T}} \\ [z_0^{\mathrm{T}}, z_1^{\mathrm{T}}]^{\mathrm{T}} &= \Gamma_0[z_0^{\mathrm{T}}, z_f^{\mathrm{T}}, z_b^{\mathrm{T}}]^{\mathrm{T}}, [u_0^{\mathrm{T}}, u_1^{\mathrm{T}}]^{\mathrm{T}} = \Gamma_i[u_0^{\mathrm{T}}, u_f^{\mathrm{T}}, u_c^{\mathrm{T}}]^{\mathrm{T}} \end{aligned}$$

and

$$\bar{A} := \Gamma_s^{-1} (A - B_0 C_0) \Gamma_s = \begin{bmatrix} A_{aa}^+ & L_{ab}^+ C_b & 0 & 0 & L_{af}^+ C_f \\ 0 & A_{bb} & 0 & 0 & L_{bf} C_f \\ 0 & L_{ab}^- C_b & A_{aa}^- & 0 & L_{af}^- C_f \\ B_c E_{ca}^+ & L_{cb} C_b & B_c E_{ca}^- & A_{cc} & L_{cf} C_f \\ B_f E_{fa}^+ & B_f E_{fb} & B_f E_{fa}^- & B_f E_{fc} & A_{ff} \end{bmatrix}$$
(3.4)

$$\bar{B} := \Gamma_s^{-1} [B_0 \ B_1] \Gamma_i = \begin{bmatrix} B_{0a}^+ & 0 & 0 \\ B_{0b}^- & 0 & 0 \\ B_{0a}^- & 0 & 0 \\ B_{0c}^- & 0 & B_c \\ B_{0f}^- & B_f^- & 0 \end{bmatrix}$$
(3.5)

$$\bar{C} := \Gamma_0^{-1} \begin{bmatrix} C_0 \\ C_1 \end{bmatrix} \Gamma_s = \begin{bmatrix} C_{0a}^+ & C_{0b} & C_{0a}^- & C_{0c} & C_{0f} \\ 0 & 0 & 0 & 0 & C_f \\ 0 & C_b & 0 & 0 & 0 \end{bmatrix}$$
(3.6)

and

$$\overline{D} := \Gamma_0^{-1} D \Gamma_i = \begin{bmatrix} I_r & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$
(3.7)

where the pair  $(A_{cc}, B_c)$  is controllable, pair  $(A_{bb}, C_b)$  is observable and the subsystem  $(A_{ff}, B_f, C_f)$  is invertible with no invariant zeros.

The proof of this theorem can be found in Sannuti and Saberi (1987) and Saberi and Sannuti (1990). We also note that the output transformation  $\Gamma_0$  is of form

$$\Gamma_0 = \begin{bmatrix} I_r & 0\\ 0 & \Gamma_{0r} \end{bmatrix}$$
(3.8)

In what follows, we state some important properties of the s.c.b which are pertinent to our present work. For further details regarding s.c.b and its properties, interested readers are referred to Saberi *et al.* (1991).

**Property 3.1:** The given system (A, B, C, D) is right-invertible if and only if  $x_b$  and hence  $z_b$  are non-existent, left-invertible if and only if  $x_c$  and hence  $u_c$  are non-existent, invertible if and only if both  $x_c$  and  $x_b$  are non-existent.

**Property 3.2:** Invariant zeros of (A, B, C, D) are the eigenvalues of  $A_{aa}^-$  and  $A_{aa}^+$ . Moreover, the stable and unstable invariant zeros of (A, B, C, D) are the eigenvalue of  $A_{aa}^-$  and  $A_{aa}^+$  respectively.

**Property 3.3:** The pair (A, B) is stabilizable if and only if  $(A_{con}, B_{con})$  is stabilizable where

$$A_{\rm con} = \begin{bmatrix} A_{aa}^+ & L_{ab}^+ C_b \\ 0 & A_{bb} \end{bmatrix}, \quad B_{\rm con} = \begin{bmatrix} B_{0a}^+ & L_{af}^+ \\ B_{0b} & L_{bf} \end{bmatrix}$$
(3.9)

There are interconnections between the s.c.b and various invariant and almost-invariant geometric subspaces. We list in the following the geometrical interpretations of some state vector components of s.c.b.

## **Property 3.4:**

- (1)  $x_a^- \oplus x_a^+ \oplus x_c$  spans  $\mathcal{V}^*(A, B, C, D)$ .
- (2)  $x_a^- \oplus x_c$  spans  $\mathcal{V}^-(A, B, C, D)$ .
- (3)  $x_a^+ \oplus x_c$  spans  $\mathcal{V}^+(A, B, C, D)$ .
- (4)  $x_c \oplus x_f$  spans  $\mathscr{G}^*(A, B, C, D)$ .
- (5)  $x_a^- \oplus x_c \oplus x_f$  spans  $\mathscr{G}^+(A, B, C, D)$ .
- (6)  $x_a^+ \oplus x_c \oplus x_f$  spans  $\mathscr{G}^-(A, B, C, D)$ .

#### 3.2. Stoorvogel's theorem

We recall in this subsection a main theorem of Stoorvogel (1991) that will play an important role in our present work. Before we introduce the theorem, let us define the following quadratic matrices,

$$F_{\gamma}(P) := \begin{bmatrix} A^{\mathrm{T}}P + PA + C_{2}^{\mathrm{T}}C_{2} + \gamma^{-2}PEE^{\mathrm{T}}P & PB + C_{2}^{\mathrm{T}}D_{2} \\ B^{\mathrm{T}}P + D_{2}^{\mathrm{T}}C_{2} & D_{2}^{\mathrm{T}}D_{2} \end{bmatrix}$$
(3.10)

and

$$G_{\gamma}(Q) := \begin{bmatrix} AQ + QA^{\mathrm{T}} + EE^{\mathrm{T}} + \gamma^{-2}QC_{2}^{\mathrm{T}}C_{2}Q & QC_{1}^{\mathrm{T}} + ED_{1}^{\mathrm{T}} \\ C_{1}Q + D_{1}E^{\mathrm{T}} & D_{1}D_{1}^{\mathrm{T}} \end{bmatrix}$$
(3.11)

It should be noted that the above matrices are dual of each other. In addition to these two matrices, we define two polynomial matrices whose role is again completely dual.

$$L(P, s) := [sI - A - \gamma^{-2} E E^{\mathrm{T}} P - B]$$
(3.12)

and

$$M(Q, s) := \begin{bmatrix} sI - A - \gamma^{-2}QC_2^{\mathrm{T}}C_2 \\ -C_1 \end{bmatrix}$$
(3.13)

Now we are ready to introduce the theorem of Stoorvogel (1991). We have the following theorem.

**Theorem 3.2:** Consider system (2.1). Assume that  $(A, B, C_2, D_2)$  and  $(A, E, C_1, D_1)$  have no invariant zeros in  $\mathbb{C}^0$ . Then the following statements are equivalent.

- (1) There exists a linear, time-invariant and proper dynamic compensator  $F_0(s)$  such that by applying  $u(s) = F_0(s)y(s)$  in (2.1) the resulting closed-loop system is internally stable. Moreover, the  $H_{\infty}$ -norm of the closed-loop transfer function from the disturbance input w to the controlled output z is less than  $\gamma$ .
- (2) There exist positive semi-definite solutions P, Q of the quadratic matrix inequalities  $F_{\gamma}(P) \ge 0$  and  $G_{\gamma}(Q) \ge 0$  satisfying  $\rho(PQ) < \gamma^2$ , such that the following rank conditions are satisfied:

(a) rank 
$$\{F_{\gamma}(P)\}$$
 = normrank  $\{G_2(s)\}$   
(b) rank  $\{G_{\gamma}(Q)\}$  = normrank  $\{G_1(s)\}$   
(c) rank  $\begin{bmatrix} L(P, s) \\ F_{\gamma}(P) \end{bmatrix}$  =  $n$  + normrank  $\{G_2(s)\}, \forall s \in \mathbb{C}^0 \cup \mathbb{C}^+$   
(d) rank  $[M(Q, s), G_{\gamma}(Q)]$  =  $n$  + normrank  $\{G_1(s)\}, \forall s \in \mathbb{C}^0 \cup \mathbb{C}^+$ 

where  $G_1(s) = C_1(sI - A)^{-1}E + D_1$ ,  $G_2(s) = C_2(sI - A)^{-1}B + D_2$  and 'normrank' denotes the rank of a matrix with entries in the field of rational functions.

**Proof:** For the proof see Stoorvogel (1991).

#### 4. Computational algorithm for $\gamma_0^*$

The algorithm for  $\gamma_0^*$  involves the computation of two non-negative scalars  $\gamma_p^*$ and  $\gamma_0^*$  which are respectively the infima in  $H_{\infty}$ -optimization of the system  $\Sigma$ 

and its dual, where in each case the measurement output is replaced by the system state. Computation of  $\gamma_P^*$  and  $\gamma_Q^*$  provides the necessary preliminary for the computation of  $\gamma_Q^*$ .

The following § 4.1 and 4.2 deal with the definition and computation of  $\gamma_P^*$  and  $\gamma_Q^*$  respectively, while in § 4.3 we present our main theorem regarding the computation of  $\gamma_Q^*$ .

## 4.1 Computation of $\gamma_{P}^{*}$

We define non-negative scalar  $\gamma_P^*$  as the infimum of  $H_{\infty}$ -optimization for the system,

$$\Sigma_{\rm P}:\begin{cases} \dot{x} = Ax + Bu + Ew\\ y = x\\ z = C_2 x + D_2 u \end{cases}$$
(4.1)

By definition,  $\gamma_P^*$  is clearly equal to  $\gamma_s^*$ . However we use the terms  $\gamma_P^*$  and  $\gamma_Q^*$  in the next subsection to conform with the notation of matrix inequalities in Stoorvogel's theorem. In what follows, we introduce a step-by-step procedure to compute  $\gamma_P^*$ .

#### Step 1

Transform the system  $(A, B, C_2, D_2)$  into the special coordinate basis (s.c.b) described in § 3. To all sub-matrices and transformations in the s.c.b of  $\Sigma_P$ , we append the subscript '<sub>P</sub>' to signify their relation to the system  $\Sigma_P$ . Next we compute

$$\Gamma_{sP}^{-1}E = [(E_{aP}^{+})^{\mathrm{T}} \quad (E_{bP})^{\mathrm{T}} \quad (E_{aP}^{-})^{\mathrm{T}} \quad (E_{cP})^{\mathrm{T}} \quad (E_{fP})^{\mathrm{T}}]^{\mathrm{T}}$$
(4.2)

It is simple to verify from the properties of s.c.b that the assumption (A2) implies  $E_{bP} = 0$ . Also, for economy of notation, we denote  $n_P$  the dimension of  $\mathbb{R}^n/\mathcal{G}^+(A, B, C_2, D_2)$ . We note that  $n_P = 0$  if and only if the system  $(A, B, C_2, D_2)$  is right-invertible and is of minimum phase.

## Step 2

If the system  $(A, B, C_2, D_2)$  is of non-minimum phase and/or not right invertible, we define

$$A_{11P} := \begin{bmatrix} A_{aaP}^{+} & L_{abP}^{+}C_{bP} \\ 0 & A_{bbP} \end{bmatrix}, \quad B_{11P} := \begin{bmatrix} B_{0aP}^{+} \\ B_{0bP} \end{bmatrix}, \quad A_{13P} := \begin{bmatrix} L_{afP}^{+} \\ L_{bfP} \end{bmatrix}$$
$$C_{21P} := \Gamma_{0rP} \begin{bmatrix} 0 & 0 \\ 0 & C_{bP} \end{bmatrix}, \quad C_{23P} := \Gamma_{0rP} \begin{bmatrix} C_{fP}C_{fP}^{T} \\ 0 \end{bmatrix}$$

and

$$A_{\rm P} := A_{11\rm P} - A_{13\rm P} (C_{23\rm P}^{\rm T} C_{23\rm P})^{-1} C_{23\rm P}^{\rm T} C_{21\rm P}$$
  

$$B_{\rm P} B_{\rm P}^{\rm T} := B_{11\rm P} B_{11\rm P}^{\rm T} + A_{13\rm P} (C_{23\rm P}^{\rm T} C_{23\rm P})^{-1} A_{13\rm P}^{\rm T}$$
  

$$C_{\rm P}^{\rm T} C_{\rm P} := C_{21\rm P}^{\rm T} C_{21\rm P} + C_{21\rm P}^{\rm T} C_{23\rm P} (C_{23\rm P}^{\rm T} C_{23\rm P})^{-1} C_{23\rm P}^{\rm T} C_{21\rm P}$$

Then we solve for the positive definite solution  $S_P$  of the algebraic matrix Riccati equation,

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$$A_{\rm P}S_{\rm P} + S_{\rm P}A_{\rm P}^{\rm T} - B_{\rm P}B_{\rm P}^{\rm T} + S_{\rm P}C_{\rm P}^{\rm T}C_{\rm P}S_{\rm P} = 0$$
(4.3)

together with the matrix  $T_{\rm P}$  defined by

$$T_{\mathbf{P}} := \begin{bmatrix} T_{aa\mathbf{P}} & 0\\ 0 & 0 \end{bmatrix}$$

where  $T_{aaP}$  is the unique solution of the algebraic matrix Lyapunov equation,

$$A_{aaP}^{+}T_{aaP} + T_{aaP}(A_{aaP}^{+})^{\mathrm{T}} = E_{aP}^{+}(E_{aP}^{+})^{\mathrm{T}}$$
(4.4)

Here we note that  $(-A_P, C_P)$  is detectable since  $-A_{aaP}$  is stable and  $(A_{bbP}, C_{bP})$  is observable. Also, the assumption (A1) implies that  $(A_P, B_P)$  is stabilizable. Hence the existence and uniqueness of the solutions  $S_P$  and  $T_{aaP}$  follow from the results of Richardson and Kwong (1986).

Step 3

The scalar  $\gamma_p^*$  is given by

$$\gamma_{\rm P}^* = \begin{cases} \sqrt{\lambda_{\rm max}(T_{\rm P}S_{\rm P}^{-1})} & \text{if } n_{\rm P} > 0\\ 0 & \text{if } n_{\rm P} = 0 \end{cases}$$
(4.5)

Here we note that the eigenvalues of  $(T_P S_P^{-1})$  are real and non-negative. (It is shown in Wielandt (1973) that AB has as many positive, zero and negative eigenvalues as A, if A is hermitian and B is hermitian and positive definite.)

**Theorem 4.1:** Consider the system  $\Sigma_{\rm P}$  given by (4.1). Then under the assumptions (A1) and (A2),

- (1)  $\gamma_{\rm P}^*$  is the infimum of  $H_{\infty}$ -optimization for  $\Sigma_{\rm P}$ .
- (2) for  $\gamma > \gamma_{P}^{*}$ , the positive semi-definite matrix  $P(\gamma)$  given by

$$P(\gamma) = (\Gamma_{sP}^{-1})^{\mathrm{T}} \begin{bmatrix} P_0(\gamma) & 0\\ 0 & 0 \end{bmatrix} \Gamma_{sP}^{-1}$$
(4.6)

where

$$P_0(\gamma) = \begin{cases} (S_{\rm P} - \gamma^{-2} T_{\rm P})^{-1} & \text{if } n_{\rm P} > 0\\ 0 & \text{if } n_{\rm P} = 0 \end{cases}$$
(4.7)

is the unique solution of the matrix inequality  $F_{\gamma}(P(\gamma)) \ge 0$  and satisfies both rank conditions (a) and (c) of Theorem 3.2. Moreover, such a solution  $P(\gamma)$  does not exist when  $\gamma < \gamma_{P}^{*}$ .

**Proof:** This is a slight generalization of the result in Chen *et al.* (1990). It can be easily shown following arguments similar to those in Chen *et al.* (1990).  $\Box$ 

**Remark 4.1:** Note that item (2) of the above theorem implies that  $\gamma_0^* \ge \gamma_P^*$ . We would also like to note that a similar result was obtained by Scherer (1990) under the assumption that the system  $(A, B, C_2, D_2)$  has no infinite zeros.  $\Box$ 

The next lemma provides the necessary and sufficient condition for  $\gamma_P^* = 0$ .

**Lemma 4.1:**  $\gamma_P^* = 0$  if and only if  $\operatorname{Im}(E) \subseteq \mathcal{G}^+(A, B, C_2, D_2)$ .

**Proof:** Again, this is a slight generalization of the result in Chen *et al.* (1990). In fact, the above result still holds when assumption (A2) is removed.  $\Box$ 

#### 4.2. Computation of $\gamma_0^*$

As in the definition of  $\gamma_P^*$ , the non-negative scalar  $\gamma_Q^*$  is defined as the infimum in  $H_{\infty}$ -optimization for the dual system,

$$\Sigma_{Q} : \begin{cases} \dot{x} = A^{T}x + C_{1}^{T}u + C_{2}^{T}w \\ y = x \\ z = E^{T}x + D_{1}^{T}u \end{cases}$$
(4.8)

Determination of  $\gamma_{0}^{*}$  follows exactly the procedure described in § 4.1 for the computation of  $\gamma_{1}^{*}$  where it now applies to the subsystem  $\Sigma_{Q}$  of (4.8). For completeness and to define properly matrices required in the computation  $\gamma_{0}^{*}$  and in our main theorem of § 4.3, we re-iterate here the three steps involved in the computation of  $\gamma_{0}^{*}$ .

#### Step 1

Transform the system  $(A^{T}, C_{1}^{T}, E^{T}, D_{1}^{T})$  into the special coordinate basis (s.c.b) described in § 3. Again we add here the subscript '<sub>Q</sub>' to all submatrices and transformations in the s.c.b of the system  $\Sigma_{Q}$ . Next we compute

$$\Gamma_{sQ}^{-1}C_2^{\rm T} = [(E_{aQ}^+)^{\rm T} \ (E_{bQ})^{\rm T} \ (E_{aQ}^-)^{\rm T} \ (E_{cQ})^{\rm T} \ (E_{fQ})^{\rm T}]^{\rm T}$$
(4.9)

It is simple to show from the properties of s.c.b that the assumption (B2) implies  $E_{bQ} = 0$ . Again, for the economy of notation, we denote  $n_Q$  the dimension of  $\mathcal{V}^+(A, E, C_1, D_1)$ . Note that  $n_Q = 0$  if and only if the system  $(A, E, C_1, D_1)$  is left-invertible and is of minimum phase.

#### Step 2

If the system  $(A, E, C_1, D_1)$  is of non-minimum phase and/or not left invertible, we define

$$A_{11Q} := \begin{bmatrix} A_{aaQ}^+ & L_{abQ}^+ C_{bQ} \\ 0 & A_{bbQ} \end{bmatrix}, \quad B_{11Q} := \begin{bmatrix} B_{0bQ}^+ \\ B_{0bQ} \end{bmatrix}, \quad A_{13Q} := \begin{bmatrix} L_{afQ}^+ \\ L_{bfQ} \end{bmatrix}$$
$$C_{21Q} := \Gamma_{0rQ} \begin{bmatrix} 0 & 0 \\ 0 & C_{bQ} \end{bmatrix}, \quad C_{23Q} := \Gamma_{0rQ} \begin{bmatrix} C_{fQ} C_{fQ}^T \\ 0 \end{bmatrix}$$

and

$$A_{Q} := A_{11Q} - A_{13Q} (C_{23Q}^{T} C_{23Q})^{-1} C_{23Q}^{T} C_{21Q}$$
$$B_{Q} B_{Q}^{T} := B_{11Q} B_{11Q}^{T} + A_{13Q} (C_{23}^{T} C_{23Q})^{-1} A_{13Q}^{T}$$
$$C_{Q}^{T} C_{Q} := C_{21Q}^{T} C_{21Q} + C_{21Q}^{T} C_{23Q} (C_{23Q}^{T} C_{23Q})^{-1} C_{23Q}^{T} C_{21Q}$$

Then we solve for the positive definite solution  $S_Q$  of the algebraic matrix Riccati equation,

$$A_{\rm Q}S_{\rm Q} + S_{\rm Q}A_{\rm Q}^{\rm T} - B_{\rm Q}B_{\rm Q}^{\rm T} + S_{\rm Q}C_{\rm Q}^{\rm T}C_{\rm Q}S_{\rm Q} = 0$$
(4.10)

together with the matrix  $T_0$  defined by

$$T_{\mathbf{Q}} := \begin{bmatrix} T_{aa\mathbf{Q}} & 0\\ 0 & 0 \end{bmatrix}$$

where  $T_{aaQ}$  is the unique solution of the algebraic matrix Lyapunov equation,

$$A_{aaQ}^{+}T_{aaQ} + T_{aaQ}(A_{aaQ}^{+})^{\mathrm{T}} = E_{aQ}^{+}(E_{aQ}^{+})^{\mathrm{T}}$$
(4.11)

Again, existence of the solutions for  $S_Q$  and  $T_Q$  follows from the assumption (B1) and the properties of s.c.b.

Step 3

The scalar  $\gamma_Q^*$  is given by

$$\gamma_Q^* = \begin{cases} \sqrt{\lambda_{\max}} (T_Q S_Q^{-1}) & \text{if } n_Q > 0\\ 0 & \text{if } n_Q = 0 \end{cases}$$
(4.12)

We note that the eigenvalues of  $(T_0 S_0^{-1})$  are real and non-negative.

**Theorem 3.2:** Consider the system  $\Sigma_Q$  given by (4.8). Then under the assumptions (B1) and (B2),

- (1)  $\gamma_{Q}^{*}$  is the infimum of  $H_{\infty}$ -optimization for  $\Sigma_{Q}$ .
- (2) for  $\gamma > \gamma_Q^*$ , the positive semi-definite matrix  $Q(\gamma)$  given by

$$Q(\gamma) = (\Gamma_{sQ}^{-1})^{\mathrm{T}} \begin{bmatrix} Q_0(\gamma) & 0\\ 0 & 0 \end{bmatrix} \Gamma_{sQ}^{-1}$$
(4.13)

where

$$Q_0(\gamma) = \begin{cases} (S_Q - \gamma^{-2} T_Q)^{-1} & \text{if } n_Q > 0\\ 0 & \text{if } n_Q = 0 \end{cases}$$
(4.14)

is the unique solution of the matrix inequality  $G_{\gamma}(Q(\gamma)) \ge 0$  and satisfies both rank conditions (b) and (d) of Theorem 3.2. Moreover, such a solution  $Q(\gamma)$  does not exist when  $\gamma < \gamma_{0}^{*}$ .

**Proof:** This is a dual version of Theorem 4.1.

**Remark 4.2:** Note that item (2) of the above theorem also implies that  $\gamma_0^* \ge \gamma_Q^*$ .

Again analogous to Lemma 4.1 we have

**Lemma 4.2:**  $\gamma_Q^* = 0$  if and only if  $\mathcal{V}^+(A, E, C_1, D_1) \subseteq \text{Ker}(C_2)$ .

**Proof:** This is a dual version of Lemma 4.1. Again, the result is still true when assumption (B2) is removed.  $\Box$ 

#### 4.3. Computation of $\gamma_0^*$

In this subsection, we provide our main results on a simple and non-iterative procedure for the computation of  $\gamma_0^*$ . First of all, we reformulate the computation of  $\gamma_0^*$  in the following lemma.

**Lemma 4.3:** Let  $\gamma_{PQ}^* = \max{\{\gamma_P^*, \gamma_Q^*\}}$ . Then

$$\gamma_0^* = \inf \left\{ \gamma \in (\gamma_{PQ}^* \infty) | f(\gamma) < \gamma^2 \right\}$$
(4.15)

where  $f(\gamma) = \rho[P(\gamma)Q(\gamma)]$ , and  $P(\gamma)$  and  $Q(\gamma)$  are given by (4.6) and (4.13) respectively.

**Proof:** It follows from Remarks 4.1 and 4.2 that  $\gamma_0^* \ge \gamma_{PQ}^*$ . Next, for any  $\hat{\gamma} \in (\gamma_{PQ}^*, \infty)$  such that  $f(\hat{\gamma}) < \hat{\gamma}^2$ , i.e.  $\rho[P(\hat{\gamma})Q(\hat{\gamma})] < \hat{\gamma}^2$ , then the corresponding  $P(\hat{\gamma})$  and  $Q(\hat{\gamma})$  as given in (4.6) and (4.13) satisfy the conditions of Theorem 3.2. Hence,  $\hat{\gamma} > \gamma_0^*$ .

One straightforward computation of  $\gamma_0^*$  can be done via an iterative search algorithm that involves in each step the multiplication of two matrices  $P(\gamma)$  and  $Q(\gamma)$  of dimensions  $n \times n$  and the determination of the spectral radius of the product  $P(\gamma)Q(\gamma)$ . This iterative search is costly and usually involves computation of eigenvalues of stiff matrices since the product  $P(\gamma)Q(\gamma)$  could become ill-conditioned as  $\gamma$  approaches  $\gamma_{PQ}^*$  from above. Hence, the overall procedure tends to be ill-conditioned. Note that as  $\gamma$  gets close to  $\gamma_P^*$ ,  $P(\gamma)$ contains the inverse of an amost singular submatrix and, similarly  $Q(\gamma)$  contains the inverse of an almost singular submatrix as  $\gamma$  approaches  $\gamma_Q^*$  (see (4.6) and (4.13)).

In contrast to the above iterative procedure, here we present an elegant, well-conditioned and non-iterative algorithm for the exact computation of  $\gamma_0^*$ . First we derive an explicit expression for  $f(\gamma)$  using (4.6) and (4.13). Then in the case where min  $\{n_P, n_Q\} > 0$ , we partition the product of the inverses of the s.c.b state transformations as follows,

$$\Gamma_{sP}^{-1}(\Gamma_{sQ}^{-1})^{\mathrm{T}} = \begin{bmatrix} \Gamma & \star \\ \star & \star \end{bmatrix}$$
(4.16)

where  $\Gamma$  is of dimension  $n_{\rm P} \times n_{\rm Q}$ .

It is then straightforward to show that the scalar function  $f(\gamma)$  is given by

$$f(\gamma) = \begin{cases} \lambda_{\max} [(S_{\rm P} - \gamma^{-2} T_{\rm P})^{-1} \Gamma(S_{\rm Q} - \gamma^{-2} T_{\rm Q})^{-1} \Gamma^{\rm T}] & \text{if } \min\{n_{\rm P}, n_{\rm Q}\} > 0\\ 0 & \text{if } \min\{n_{\rm P}, n_{\rm Q}\} = 0 \end{cases}$$
(4.17)

The function  $f(\gamma)$  of (4.17) is a well-defined mapping from  $(\gamma_{PQ}^*, \infty)$  to  $[0, \infty)$ . Its evaluation involves the computation of the maximum eigenvalue of a matrix of dimension  $n_P \times n_P$ , which is normally of a much smaller dimension than the original product  $P(\gamma)Q(\gamma)$ . We establish some important properties of the function  $f(\gamma)$  in the following proposition.

**Proposition 4.1:**  $f(\gamma)$  is a continuous, non-negative and non-increasing function of  $\gamma$  on  $(\gamma_{PO}^*, \infty)$ .

**Proof:** The proof follows from Observation 4.1 of Chen *et al.* (1992).

The function  $f(\gamma)$  defined above can be extended as a mapping from  $[\gamma_{PQ}^*, \infty)$  to  $[0, \infty)$  by setting  $f(\gamma_{PQ}^*) = \lim_{\gamma \to \gamma_{PQ}^*} f(\gamma)$ . It follows from Proposition 4.1 that the limit  $f(\gamma_{PQ}^*)$  exists and could be finite or infinite.

Before stating our main result of this subsection regarding the computation of  $\gamma_0^*$ , we need to establish several important propositions.

**Proposition 4.2:**  $f(\gamma) = \gamma^2$  has either no solution or a unique solution in the interval  $(\gamma_{PO}^*, \infty)$ .

**Proof:** The result follows from Proposition 4.1 and the fact that  $\gamma^2$  is strictly increasing for positive  $\gamma$ .

**Proposition 4.3:** If  $f(\gamma) = \gamma^2$  has no solution in the interval  $(\gamma_{PQ}^*, \infty)$  then  $\gamma_0^*$  is equal to  $\gamma_{PQ}^*$ . Otherwise,  $\gamma_0^*$  is equal to the unique solution of  $f(\gamma) = \gamma^2$  in the interval  $(\gamma_{PQ}^*, \infty)$ .

**Proof:**  $f(\gamma) = \gamma^2$  has no solution in the interval  $(\gamma_{PQ}^*, \infty)$  implies that  $f(\gamma) < \gamma^2$  for all  $\gamma \in (\gamma_{PQ}^*, \infty)$  and hence according to Lemma 4.3,  $\gamma_0^* = \gamma_{PQ}^*$ . On the other hand, it is obvious that  $\gamma_0^*$  is equal to the unique solution of  $f(\gamma) = \gamma^2$  when such a solution exists.

At a first glance, it seems that the solution of  $f(\gamma) = \gamma^2$  would involve the rooting of a highly nonlinear algebraic equation in  $\gamma$ . Actually its solution can be achieved in one-step. Namely, the problem of solving  $f(\gamma) = \gamma^2$ , if such a solution exists in the interval  $(\gamma_{PQ}^*, \infty)$ , can be converted to the problem of calculating the maximum eigenvalue of a constant matrix. In fact, we also show that, when  $f(\gamma) = \gamma^2$  has no solution in the interval  $(\gamma_{PQ}^*, \infty)$ , the maximum eigenvalue of this matrix is equal to  $\gamma_{PQ}^*$ , which is  $\gamma_0^*$  as well. Define

$$N(\gamma) =: \begin{cases} (S_{\rm P} - \gamma^{-2} T_{\rm P})^{-1} \Gamma(S_{\rm Q} - \gamma^{-2} T_{\rm Q})^{-1} \Gamma^{\rm T} - \gamma^{2} I & \text{if } \min\{n_{\rm P}, n_{\rm Q}\} > 0\\ -\gamma^{2} I & \text{if } \min\{n_{\rm P}, n_{\rm Q}\} = 0 \end{cases}$$

$$(4.18)$$

and

$$M := \begin{cases} \begin{bmatrix} T_{P}S_{P}^{-1} + \Gamma S_{Q}^{-1}\Gamma^{T}S_{P}^{-1} & -\Gamma S_{Q}^{-1} \\ -T_{Q}S_{Q}^{-1}\Gamma^{T}S_{P}^{-1} & T_{Q}S_{Q}^{-1} \end{bmatrix} & \text{if } n_{P} > 0 \text{ and } n_{Q} > 0 \\ T_{P}S_{P}^{-1} & \text{if } n_{P} > 0 \text{ and } n_{Q} = 0 \\ T_{Q}S_{Q}^{-1} & \text{if } n_{P} = 0 \text{ and } n_{Q} > 0 \\ 0 & \text{if } n_{P} = 0 \text{ and } n_{Q} = 0 \end{cases}$$
(4.19)

We have the following propositions on the matrices M and  $N(\gamma)$ .

**Proposition 4.4:** Eigenvalues of M are real and non-negative.

**Proof:** It is trivial when  $\min\{n_P, n_Q\} = 0$ . For the case where  $\min\{n_P, n_Q\} > 0$ , we have

$$\lambda[M] = \lambda \left\{ \begin{bmatrix} I & 0 \\ 0 & T_{Q} \end{bmatrix} \begin{bmatrix} T_{P} + \Gamma S_{Q}^{-1} \Gamma^{T} & -\Gamma S_{Q}^{-1} \\ -S_{Q}^{-1} \Gamma^{T} & S_{Q}^{-1} \end{bmatrix} \begin{bmatrix} S_{P}^{-1} & 0 \\ 0 & I \end{bmatrix} \right\}$$
$$= \lambda \left\{ \begin{bmatrix} S_{P}^{-1} & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} I & 0 \\ 0 & T_{Q} \end{bmatrix} \begin{bmatrix} T_{P} + \Gamma S_{Q}^{-1} \Gamma^{T} & -\Gamma S_{Q}^{-1} \\ -S_{Q}^{-1} \Gamma^{T} & S_{Q}^{-1} \end{bmatrix} \right\}$$
$$= \lambda \left\{ \begin{bmatrix} S_{P}^{-1} & 0 \\ 0 & T_{Q} \end{bmatrix} \begin{bmatrix} T_{P} + \Gamma S_{Q}^{-1} \Gamma^{T} & -\Gamma S_{Q}^{-1} \\ -S_{Q}^{-1} \Gamma^{T} & S_{Q}^{-1} \end{bmatrix} \right\}$$
(4.20)

Now, it is trivial to verify that both sub-matrices in (4.20) are symmetric and positive semidefinite. Then using the result of Weilandt (1973) (i.e. Theorem 3), it is simple to show that the eigenvalues of M are real and non-negative.

## **Proposition 4.5:**

(i)  $N(\gamma)$  has real eigenvalues for all  $\gamma \in (\gamma_{PQ}^*, \infty)$ .

(ii)  $\lambda_{\max}[N(\gamma)] = f(\gamma) - \gamma^2$  is continuous and strictly decreasing on  $(\gamma_{PQ}^*, \infty)$ .

**Proof:** Again it is trivial when  $\min\{n_P, n_Q\} = 0$ . For the case where  $\min\{n_P, n_Q\} > 0$ , we have

(i) It is straightforward to show that (S<sub>P</sub> - γ<sup>-2</sup>T<sub>P</sub>)<sup>-1</sup> > 0 and (S<sub>Q</sub> - γ<sup>-2</sup>T<sub>Q</sub>)<sup>-1</sup> > 0 for all γ ∈ (γ<sup>\*</sup><sub>PQ</sub>, ∞). Hence, all the eigenvalues of N(γ) are real for γ ∈ (γ<sup>\*</sup><sub>PQ</sub>, ∞).

(ii) It follows from Proposition 4.1.

**Proposition 4.6:** If  $\min\{n_P, n_Q\} > 0$ , then the roots of  $\det[N(\gamma)] = 0$  are real. Moreover, the largest root of  $\det[N(\gamma)] = 0$  in the interval  $(\gamma_{PQ}^*, \infty)$  is equal to  $\sqrt{\lambda_{\max}(M)}$ .

**Proof:** Using the definition of  $N(\gamma)$  in (4.18), we have

$$det[N(\gamma)] = (-1)^{n_{\rm P}} det[\gamma^2 I - (S_{\rm P} - \gamma^{-2} T_{\rm P})^{-1} \Gamma(S_{\rm Q} - \gamma^{-2} T_{\rm Q})^{-1} \Gamma^{\rm T}]$$

$$= \frac{(-1)^{n_{\rm P}}}{det[S_{\rm P} - \gamma^{-2} T_{\rm P}]} det[\gamma^2 S_{\rm P} - T_{\rm P} - \gamma^2 \Gamma(\gamma^2 S_{\rm Q} - T_{\rm Q})^{-1} \Gamma^{\rm T}]$$

$$= \frac{(-1)^{n_{\rm P}}}{det[S_{\rm P} - \gamma^{-2} T_{\rm P}] det[\gamma^2 S_{\rm Q} - T_{\rm Q}]} det\left[\frac{\gamma^2 S_{\rm P} - T_{\rm P}}{\gamma^2 \Gamma^{\rm T}} \frac{\Gamma}{\gamma^2 S_{\rm Q} - T_{\rm Q}}\right]$$

$$= \frac{(-1)^{n_{\rm P}} det[S_{\rm P}] det[S_{\rm Q}]}{det[S_{\rm P} - \gamma^{-2} T_{\rm P}] det[\gamma^2 S_{\rm Q} - T_{\rm Q}]} det[\gamma^2 I - M]$$
(4.21)

Now it is simple to see that the roots of det  $[N(\gamma)] = 0$  are real since all the roots of det  $[\gamma^2 S_P - T_P] = 0$ , det  $[\gamma^2 S_Q - T_Q] = 0$  and det  $[\gamma^2 I - M] = 0$  are real. Moreover, it follows from (4.5) and (4.12) that det  $[S_P - \gamma^{-2} T_P] \neq 0$  and det  $[\gamma^2 S_Q - T_Q] \neq 0$  for all  $\gamma \in (\gamma_{PQ}^*, \infty)$ . Hence, the largest root of det  $[N(\gamma)] = 0$  in  $(\gamma_{PQ}^*, \infty)$  is equal to the largest root of det  $[\gamma^2 I - M] = 0$ , which is equal to  $\sqrt{\lambda_{max}(M)}$ .

The main result of this subsection is summarized in the following theorem.

## Theorem 4.3:

$$\gamma_0^* = \sqrt{\lambda_{\max}(M)}$$

where M is defined in (4.19).

**Proof:** The result is obvious for the case where  $\min\{n_P, n_Q\} = 0$ . In what follows, we proceed to prove our claim for the case where  $\min\{n_P, n_Q\} > 0$ .

First, we will show that  $\gamma_0^*$  is equal to the largest root of det  $[N(\gamma)] = 0$  when  $f(\gamma) = \gamma^2$  has a unique solution in the interval  $(\gamma_{PQ}^*, \infty)$ . It is simple to observe that det  $[N(\gamma_0^*)] = 0$  since  $\lambda_{\max}[N(\gamma_0^*)] = f(\gamma_0^*) - (\gamma_0^*)^2 = 0$ . Now suppose that there exists a  $\gamma_1$  such that det  $[N(\gamma_1)] = 0$  and  $\gamma_1 > \gamma_0^*$ . This implies that there exists an eigenvalue of  $N(\gamma_1)$ , say  $\lambda_i[N(\gamma_1)]$ , such that  $\lambda_i[N(\gamma_1)] \neq \lambda_{\max}[N(\gamma_1)]$  and  $\lambda_i[N(\gamma_1)] = 0$ . Thus, we have

$$\lambda_{\max}[N(\gamma_1)] > \lambda_i[N(\gamma_1)] = 0 = \lambda_{\max}[N(\gamma_0^*)],$$

contradicting the findings in Proposition 4.5 that  $\lambda_{\max}[N(\gamma)]$  must be a non-increasing function. Hence,  $\gamma_0^*$  is the largest root of det $[N(\gamma)] = 0$  and it is equal to  $\sqrt{\lambda_{\max}(M)}$  as shown in Proposition 4.6.

Now we consider the situation when  $f(\gamma) = \gamma^2$  has no solution in the interval  $(\gamma_{PQ}^*, \infty)$ . In this case, clearly we have  $\gamma_0^* = \gamma_{PQ}^*$  and  $0 \le f(\gamma_{PQ}^*) \le (\gamma_{PQ}^*)^2$ . The last inequality and the definition of  $N(\gamma)$  in (4.18) imply that  $-(\gamma_{PQ}^*)^2 \le \lambda_i [N(\gamma_{PQ}^*)] \le 0$ . Thus, the determinant of  $N(\gamma_{PQ}^*)$  is bounded. Evaluating (4.21) at  $\gamma = \gamma_{PQ}^*$ , we have

$$\det[N(\gamma_{PQ}^{*})] \det[S_{P} - (\gamma_{PQ}^{*})^{-2}T_{P}] \det[(\gamma_{PQ}^{*})^{2}S_{Q} - T_{Q}]$$
  
=  $(-1)^{n_{P}} \det[S_{P}] \det[S_{Q}] \det[(\gamma_{PQ}^{*})^{2}I - M]$  (4.22)

Note that from (4.5) and (4.12) and the definition of  $\gamma_{PQ}^*$ , we have

$$\det[S_{\rm P} - (\gamma_{\rm PQ}^{*})^{-2}T_{\rm P}]\det[(\gamma_{\rm PQ}^{*})^{2}S_{\rm Q} - T_{\rm Q}] = 0$$

and since det  $[N(\gamma_{PO}^*)]$  is bounded, it follows from (4.22) that

$$\det\left[(\gamma_{\rm PQ}^*)^2 I - M\right] = 0$$

or  $(\gamma_{PQ}^*)^2$  is an eigenvalue of M. Furthermore since det  $[N(\gamma)] = 0$  and similarly det  $[\gamma^2 I - M] = 0$  do not have a root in  $(\gamma_{PQ}^*, \infty)$ , hence  $\gamma_{PQ}^* = \sqrt{\lambda_{max}(M)}$ .  $\Box$ 

We illustrate our main result in the following example.

Example: Consider a given system characterized by

Step 1

It is simple to verify that the subsystem  $(A, B, C_2, D_2)$  is neither left- nor right-invertible with one invariant zero at s = 1. Also, assumption (A 2) is satisfied. Moreover, it is already in the form of s.c.b with

$$A_{\mathbf{P}} = \begin{bmatrix} 1 & 1 & 1 \\ 0 & 1 & 0 \\ 0 & 1 & 0 \end{bmatrix}, \quad B_{\mathbf{P}}B_{\mathbf{P}}^{\mathsf{T}} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 2 \end{bmatrix}, \quad C_{\mathbf{P}}^{\mathsf{T}}C_{\mathbf{P}} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

and

$$A_{aaP}^{+} = 1, \quad E_{aP}^{+} = [5 \ 1]$$

Then, solving equations (4.3) and (4.4), we obtain

$$S_{\rm P} = \begin{bmatrix} 0.556281 & 0.185427 & -0.305593\\ 0.185427 & 0.395142 & 0.231469\\ -0.305593 & 0.231469 & 1.217984 \end{bmatrix}, \quad T_{\rm P} = \begin{bmatrix} 13 & 0 & 0\\ 0 & 0 & 0\\ 0 & 0 & 0 \end{bmatrix}$$

Step 2

The subsystem  $(A, E, C_1, D_1)$  is invertible and of non-minimum phase with invariant zeros at  $\{-1.630662, -3.593415, 0.521129 \pm j0.363043\}$ . Hence, assumption (B2) is automatically satisfied. Applying s.c.b transformation to  $(A^{T}, C_{1}^{T}, E^{T}, D_{1}^{T})$ , we obtain

$$\Gamma_{sQ} = \begin{bmatrix} -0.011218 & -0.106028 & -0.906482 & -0.212184 & 0.090909 \\ 0.185213 & -0.745725 & 0.194520 & -0.119195 & 0.181818 \\ -0.919232 & 0.096732 & 0.326906 & -0.603079 & 0.272727 \\ 0.279141 & 0.532936 & 0.087364 & -0.581308 & 0.181818 \\ -0.206551 & -0.373195 & 0.161098 & 0.489027 & 0.090909 \end{bmatrix}$$

 $\Gamma_{0rO} = 1$ 

 $A_{\rm Q} = A_{aa\rm Q}^{+} = \begin{bmatrix} 0.433179 & -0.253237\\ 0.551005 & 0.609080 \end{bmatrix}, \quad B_{\rm Q}B_{\rm Q}^{\rm T} = \begin{bmatrix} 0.033508\\ -0.018630 \end{bmatrix}$ -0.0186300.030289

 $C_{\rm Q}^{\rm T}C_{\rm Q} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad E_{a\rm Q}^{+} = \begin{bmatrix} -0.769496 & 0.010023 & 0.448951 \\ -0.090061 & 0.655677 & -1.044466 \end{bmatrix}$ -0.769496-0.090061

Again, solving equations (4.10) and (4.11), we obtain

$$S_{\rm Q} = \begin{bmatrix} 0.026333 & -0.021114 \\ -0.021114 & 0.043965 \end{bmatrix}, \quad T_{\rm Q} = \begin{bmatrix} 1.274771 & -0.555799 \\ -0.555799 & 1.764580 \end{bmatrix}$$

Step 3

Evaluate

$$M = 10^2 \times \begin{bmatrix} 0.500695 & -0.334250 & 0.245016 & 0.082332 & 0.052125 \\ -0.442374 & 0.992368 & -0.260321 & 0.032515 & 0.253182 \\ 0.616882 & -0.513348 & 0.588766 & 0.501907 & 0.261525 \\ 1.074941 & -1.295698 & 0.921909 & 0.622391 & 0.172484 \\ -0.583103 & 1.526365 & -0.286520 & 0.180099 & 0.487850 \end{bmatrix}$$

We obtain

 $\gamma_0^* = 13.638725$ 

## 5. Other related results

Results developed in §4 can also be used to examine solvability conditions of almost disturbance decoupling problems with internal stability and to establish exact conditions where  $\gamma_0^* = \gamma_s^*$ .

## 5.1. Almost disturbance decoupling with stability

The problem of almost disturbance decoupling was first introduced by Willems (see Weiland and Willems (1989) for a recent result and related references). The basic problem is the design of a linear time-invariant internally stabilizing controller using output feedback such that the controlled output z is approximately decoupled from the disturbance input w. The more precise definitions of these problems are given below.

**Definition 5.1:** Consider the system of (2.1) with  $C_1 = I$  and  $D_1 = 0$ , i.e., y = x. Then we say that the  $H_{\infty}$ -Almost Disturbance Decoupling Problem with internal Stability  $(\text{ADDPS})_{H_{\infty}}$  is solvable if for all  $\varepsilon > 0$  there exists a state feedback law u = Fx for the system defined above such that the closed-loop system is internally stable and the  $H_{\infty}$ -norm of the transfer function between the disturbance input w and the controlled output z is less than  $\varepsilon$ .

**Definition 5.2:** Consider the system of (2.1), we say that the  $H_{\infty}$ -Almost Disturbance Decoupling Problem with Measurement feedback and internal Stability  $(\text{ADDPMS})_{H_{\infty}}$  is solvable if for all  $\varepsilon > 0$  there exists an output feedback law  $u(s) = F_0(s)y(s)$  such that the closed-loop system is internally stable and the  $H_{\infty}$ -norm of the transfer function between the disturbance input w and the controlled output z is less than  $\varepsilon$ .

From the above formulation, it is obvious that solvability conditions for  $(ADDPS)_{H_*}$  and  $(ADDPMS)_{H_*}$  are exactly the conditions where  $\gamma_s^* = 0$  and  $\gamma_0^* = 0$  respectively. Solvability conditions for  $(ADDPS)_{H_*}$  with  $D_2 = 0$  and for  $(ADDPMS)_{H_*}$  with  $D_1 = 0$  and  $D_2 = 0$  are well-known (see Weiland and Willems 1989). In the following theorem, we extend these results to the general case when  $D_1 \neq 0$  and/or  $D_2 \neq 0$ .

**Theorem 5.1:** Consider the system  $\Sigma$  as given by (2.1). Let  $C_1 = I$  and  $D_1 = 0$ , *i.e.* y = x. Then  $(ADDPS)_{H_x}$  is solvable under the assumption (A1) if and only if  $\text{Im}(E) \subseteq \mathcal{G}^+(A, B, C_2, D_2)$ .

**Proof:** The proof follows from Lemma 4.1.

**Theorem 5.2:** Consider the system  $\Sigma$  as given by (2.1). Then  $(ADDPMS)_{H_{\omega}}$  is solvable under the assumptions (A1) and (B1) if and only if

- (1) Im  $(E) \subseteq \mathcal{G}^+(A, B, C_2, D_2),$
- (2)  $\mathscr{V}^+(A, E, C_1, D_1) \subseteq \operatorname{Ker}(C_2),$
- (3)  $\mathscr{V}^+(A, E, C_1, D_1) \subseteq \mathscr{G}^+(A, B, C_2, D_2).$

**Proof.** ( $\Rightarrow$ ): It follows from Lemmas 4.1 and 4.2 that the firt two conditions imply  $\gamma_P^* = \gamma_Q^* = 0$  and

$$T_{\rm P} = 0 \quad \text{and} \quad T_{\rm O} = 0 \tag{5.1}$$

Also, it is simple to verify that

$$\mathscr{V}^+(A, E, C_1, D_1) = \operatorname{Im}\left\{ (\Gamma_{sQ}^{-1})^{\mathrm{T}} \begin{bmatrix} I_{n_{Q}} \\ 0 \end{bmatrix} \right\}$$

and

$$\mathscr{G}^+(A, B, C_2, D_2) = \operatorname{Ker} \{ [I_{n_P} \ 0] \Gamma_{sP}^{-1} \}$$

Then, it is easy to see that the condition

$$\mathscr{V}^+(A, E, C_1, D_1) \subseteq \mathscr{G}^+(A, B, C_2, D_2)$$
 (5.2)

holds if and only if

$$\begin{bmatrix} I_{n_{P}} & 0 \end{bmatrix} \Gamma_{sP}^{-1} (\Gamma_{sQ}^{-1})^{\mathrm{T}} \begin{bmatrix} I_{n_{Q}} \\ 0 \end{bmatrix} = \Gamma = 0$$
(5.3)

Equations (5.1) to (5.3) imply that M = 0 and hence  $\gamma_0^* = 0$ .

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( $\Leftarrow$ ): Conversely, it follows from Lemma 4.3 that  $\gamma_0^* = 0$  implies  $\gamma_P^* = \gamma_0^* = 0$ . Then, by Lemmas 4.1 and 4.2, we have

$$\operatorname{Im}(E) \subseteq \mathscr{G}^+(A, B, C_2, D_2), \mathscr{V}^+(A, E, C_1, D_1) \subseteq \operatorname{Ker}(C_2)$$

and

$$T_{\rm P} = 0, \quad T_{\rm O} = 0$$

Thus,

$$M = \begin{bmatrix} \Gamma S_{\mathbf{Q}}^{-1} \Gamma^{\mathrm{T}} S_{\mathbf{P}}^{-1} & -\Gamma S_{\mathbf{Q}}^{-1} \\ 0 & 0 \end{bmatrix}$$

Now, it is simple to see that  $\gamma_0^* = \sqrt{\lambda_{\max}(M)} = 0$  implies  $\Gamma = 0$  and hence

$$\mathcal{V}^+(A, E, C_1, D_1) \subseteq \mathcal{G}^+(A, B, C_2, D_2)$$

This completes the proof of Theorem 5.2.

# 5.2. When $\gamma_0^*$ is equal to $\gamma_s^*$

An interesting question in  $H_{\infty}$ -optimization problem is under what conditions the infimum in  $H_{\infty}$ -optimization via output feedback is equal to that achieved using state feedback. In the following theorem we provide a necessary and sufficient condition under which  $\gamma_0^* = \gamma_s^*$ .

**Theorem 5.3:** Consider the system  $\Sigma$  given by (2.1) that satisfies the assumptions (A1), (A2), (B1) and (B2). Then  $\gamma_0^* = \gamma_s^*$  if and only if

$$\lambda_{\max}(M) = \begin{cases} \lambda_{\max}(T_{\mathrm{P}}S_{\mathrm{P}}^{-1}) & \text{if } n_{\mathrm{P}} > 0\\ 0 & \text{if } n_{\mathrm{P}} = 0 \end{cases}$$

**Proof:** The proof follows from Theorems 4.1 and 4.3.

#### Corollary 5.1:

- (1) If  $(A, E, C_1, D_1)$  is left-invertible and is of minimum phase, i.e.  $n_Q = 0$ , then  $\gamma_0^* = \gamma_s^*$ .
- (2) If  $(A, B, C_2, D_2)$  is right-invertible and is of minimum phase, i.e.  $n_P = 0$ , then  $\gamma_0^* = \gamma_s^*$  if and only if  $\mathcal{V}^+(A, E, C_1, D_1) \subseteq \text{Ker}(C_2)$ .
- (3) If both  $n_{\rm P}$  and  $n_{\rm Q}$  are non-zero, then  $\gamma_0^* = \gamma_s^*$  if  $\mathcal{V}^+(A, E, C_1, D_1) \subseteq \mathcal{G}^+(A, B, C_2, D_2)$  and  $\lambda_{\max}(T_{\rm Q}S_{\rm Q}^{-1}) \leq \lambda_{\max}(T_{\rm P}S_{\rm P}^{-1})$ .

**Proof:** Items (1) and (2) are obvious in view of Theorem 4.3 and Lemma 4.2. To prove item (3), let us consider the following. It follows from (5.2) and (5.3) that

$$\mathscr{V}^+(A, E, C_1, D_1) \subseteq \mathscr{G}^+(A, B, C_2, D_2)$$

implies  $\Gamma = 0$  and hence

$$M = \begin{bmatrix} T_{\mathrm{P}} S_{\mathrm{P}}^{-1} & 0\\ 0 & T_{\mathrm{Q}} S_{\mathrm{Q}}^{-1} \end{bmatrix}$$

Thus the result is trivial in view of the fact  $\gamma_P^* = \gamma_s^*$ .

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## 6. Conclusions

In this paper we have extended the results of Chen *et al.* (1992) and presented a simple and non-iterative algorithm for the computation of the infimum for a class of singular  $H_{\infty}$ -optimization problems using output feedback. We have shown that this infimum is equal to the square root of the maximum eigenvalue of a constant matrix that can be easily obtained from the system matrices of  $\Sigma$ . Our results are obtained under the assumptions that the two subsystems  $\Sigma_{\rm P}$  and  $\Sigma_{\rm O}$  have no invariant zeros on the j $\omega$  axis and satisfy certain geometric conditions. The proposed algorithm for computing the infimum is applicable to the general case of a singular  $H_{\infty}$ -optimization problem where no restrictions have been placed on the direct feedthrough matrices from the control input to the controlled output, and from the disturbance to the measurement output. Our current research effort is directed toward removing some of the assumptions imposed in this paper on  $\Sigma_{\rm P}$  and  $\Sigma_{\rm O}$ .

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#### References

- BASAR, T. S., and BERNARD, P., 1989, Differential Games and Applications. Lecture Notes in Control and Information Science, Vol. 119, (Berlin: Springer-Verlag).
- CHEN, B. M., SABERI, A., and LY, U., 1990, Exact computation of the infimum in  $H_{\infty}$ -optimization via state feedback. Proceedings of the 28th Annual Allerton Conference on Communication, Control and Computing, Monticello, Illinois, pp. 745–754 (also in: 1992, Control-Theory and Advanced Technology, 6, 17–35); 1992, Exact computation of the infimum in  $H_{\infty}$ -optimization via output feedback. IEEE Transactions on Automatic Control, **37**, 70–78.
- DOYLE, J. C., 1984, Lecture Notes in Advances in Multivariable Control (ONR/Honeywell Workshop).
- DOYLE, J. C., and GLOVER, K., 1988, State-space formulae for all stabilizing controllers that satisfy an  $H_{\infty}$ -norm bound and relations to risk sensitivity. Systems and Control Letters, 11, 167–172.
- DOYLE, J. C., GLOVER, K., KHARGONEKAR, P. P., and FRANCIS, B. A., 1989, State-space solutions to standard  $H_2$  and  $H_{\infty}$ -control problems. *IEEE Transactions on Automatic Control*, **34**, 831–847.
- FRANCIS, B. A., 1987, A Course in  $H_{\infty}$  Control Theory. Lecture Notes in Control and Information Sciences, Vol. 88 (Berlin: Springer-Verlag).
- GLOVER, K., 1984, All optimal Hankel-norm approximations of linear multivariable systems and their  $L_{\infty}$ -error bounds. *International Journal of Control*, **39**, 1115–1193.
- KHARGONEKAR, P., PETERSEN, I. R., and ROTEA, M. A., 1988,  $H_{\infty}$ -optimal control with state feedback. *IEEE Transactions on Automatic Control*, **33**, 786–788.
- PAPAVASSILOPOULOS, G. P., and SAFONOV, M. G., 1989, Robust control design via game theoretic methods. Proceedings of the 28th IEEE Conference on Decision and Control, Tampa, Florida, pp. 382-387.
- PETERSEN, I. R., 1987, Disturbance attenuation and H<sub>∞</sub>-optimization: a design method based on the algebraic Riccati equation. *IEEE Transactions on Automatic Control*, 32, 427-429; 1988, Complete results for a class of state feedback disturbance attenuation problems. *Proceedings of the 27th IEEE Conference on Decision and Control*, Austin, Texas, pp. 1349-1353.

- RICHARDSON, T. J., and KWONG, R. H., 1986, On positive definite solutions to the algebraic Riccati equation. Systems and Control Letters, 7, 99-104.
- SABERI, A., CHEN, B. M., and SANNUTI, P., 1991, Theory of LTR for nonminimum phase systems, recoverable target loops, recovery in a subspace. Part 1: Analysis. International Journal of Control, 53, 1067-1115.
- SABERI, A., and SANNUTI, P., 1990, Squaring down of non-strictly proper systems. International Journal of Control, 51, 621-629.
- SAMPEI, M., MITA, T., and NAKAMICHI, M., 1990, An algebraic approach to  $H_{\infty}$ -output feedback control problem. Systems and Control Letters, 14, 13–24.
- SANNUTI, P., and SABERI, A., 1987, A special coordinate basis of multivariable linear systems-finite and infinite zero structure, squaring down and decoupling. *International Journal of Control*, 45, 1655-1704.
- SCHERER, C., 1990,  $H_{\infty}$ -control by state-feedback and fast algorithm for the computation of optimal  $H_{\infty}$ -norms. *IEEE Transactions on Automatic Control*, 35, 1090–1099.
- STOORVOGEL, A. A., 1991, The singular  $H_{\infty}$ -control problem with dynamic measurement feedback. SIAM Journal on Control and Optimization, 29, 160–184.
- STOORVOGEL, A. A., and TRENTELMAN, H. L., 1990, The quadratic matrix inequality in singular  $H_{\infty}$ -control with state feedback. SIAM Journal on Control and Optimization, 28, 1190-1208.
- WEILAND, S., and WILLEMS, J. C., 1989, Almost disturbance decoupling with internal stability. *IEEE Transactions on Automatic Control*, 34, 277–286.
- WIELANDT, H., 1973, On the eigenvalues of A + B and AB, Journal of Research of the National Bureau of Standards-B. Mathematical Science, 778, 61-63.
- ZAMES, G., 1981, Feedback and optimal sensitivity: model reference transformations, multiplicative seminorms, and approximate inverses. *IEEE Transactions on Automatic Control*, 26, 301-320.
- ZHOU, K., and KHARGONEKAR, P. P., 1988, An algebraic Riccati equation approach to  $H_{\infty}$ -optimization. Systems and Control Letters, 11, 85-91.