Linear systems toolkit in Matlab: structural decompositions and their applications

Xinmin LIU¹, Ben M. CHEN², Zongli LIN¹

- (1. Charles L. Brown Department of Electrical and Computer Engineering, University of Virginia, Charlottesville, USA;
- 2. Department of Electrical and Computer Engineering, National University of Singapore, Singapore 117576, Singapore)

Abstract: This paper presents a brief description of the software toolbox, linear systems toolkit, developed in Matlab environment. The toolkit contains 66 m-functions, including structural decompositions of linear autonomous systems, unforced/unsensed systems, proper systems, and singular systems, along with their applications to system factorizations, sensor/actuator selection, H-two and H-infinity control, and disturbance decoupling problems.

Keywords: Linear systems; Structural decompositions; Linear control; Software development

1 Introduction

The state space representation of linear multivariable systems is fundamental to the analysis and design of dynamical systems. Modern control theory relies heavily on the state space representation of dynamical systems, which facilitates characterization of the inherent properties of dynamical systems. Since the introduction of the concept of the state, the study of linear systems in the state space representation itself has emerged as an ever active research area, covering a wide range of topics from the basic notions of stability, controllability, observability, redundancy and minimality to more intricate properties of finite and infinite zero structures, invertibility, and geometric subspaces. A deeper understanding of linear systems facilitates the development of modern control theory. The demanding expectations from modern control theory impose an ever increasing demand for the understanding and utilization of subtler properties of linear systems.

Structural properties play an important role in our understanding of linear systems in the state space representation. The structural canonical form representation of linear systems not only reveals the structural properties but also facilitates the design of feedback laws that meet various control objectives. In particular, it decomposes the system into various subsystems. These subsystems, along with the interconnections that exist among them, clearly show the structural properties of the system. The simplicity of the subsystems and their explicit interconnections with

each other lead us to a deeper insight into how feedback control would take effect on the system, and thus to the explicit construction of feedback laws that meet our design specifications. The search for structural canonical forms and their applications in feedback design for various performance specifications has been an active area of research for a long time. The effectiveness of the structural decomposition approach has also been extensively explored in nonlinear systems and control theory in the recent past.

In this article, we present a MATLAB toolkit, linear systems toolkit, for realizing various structural decomposition techniques recently reported in a monograph by Chen, Lin and Shamash [1]. The toolkit [2], which has been built upon the earlier versions [3,4], is able to efficiently compute the structural decompositions of autonomous systems, unforced/unsensed systems, proper systems, and singular systems, along with their properties, such as finite and infinite zero structures, invertibility structures and geometric subspaces. The applications decomposition techniques to system factorizations, structural assignments via sensor or actuator selection, and H2 and H_{∞} control are also included. It is now used extensively in the education and research of control theory. Its rich collection of linear algebra functions are immediately useful to the control engineer and system analyst. Its easy-to-use environment allows the problems and solutions to be expressed in familiar mathematical notation.

The detailed algorithms and proofs of the functions reported in the toolkit can be found in the monograph of

Chen, Lin and Shamash [1], and the beta version of this toolkit is currently available on the website at http://linearsystemskit.net or http://hdd.ece.nus.edu.sg/~ bmchen. Readers who have our earlier versions [3,4] of the software realization of the special coordinate basis of Sannuti and Saberi [6] are strongly encouraged to update to the new toolkit. The special coordinate basis, implemented in the new toolkit, is based on a numerically stable algorithm recently reported in Chu, Liu and Tan [5], together with an enhanced procedure reported in [1].

The paper is organized as follows. Section 2 provides the detailed list of m-functions in the toolkit. Section 3 describes some key functions of the toolkit, while Section 4 demonstrates some m – functions with numerical examples. Finally, Section 5 draws a brief conclusion to the paper.

2 Contents of tookit

We list in this section the detailed contents of the toolkit. We note that some m-functions in the toolkit are interactive, which require users to enter desired parameters during execution. Others are implemented in a way that can return results either in a symbolic or numerical form.

The current version of the toolkit consists of the following m-functions:

A) Decompositions of autonomous systems.

- 1) ssd: continuous-time stability structural decomposition:
 - 2) dssd: discrete-time stability structural decomposition;
 - 3) jcf: Jordan canonical form;
 - 4) rjd: real Jordan decomposition.

B) Decompositions of unforced and unsensed systems.

- 1) osd: observability structural decomposition;
- 2) obvidx: observability index;
- 3) bdosd: block diagonal observable structural decomposition;
 - 4) csd: controllability structural decomposition;
 - 5) ctridx: controllability index;
- 6) bdcsd: block diagonal controllable structural decomposition.

C) Decompositions & structural properties of proper system.

- 1) scbraw: raw decomposition without integration chains;
- 2) scb: decomposition of a continuous-time system;
- 3) dscb: decomposition of a discrete-time system;
- 4) kcf: Kronecker canonical form for system matrices;

- 5) morseidx: Morse indices;
- 6) blkz: blocking zeros;
- 7) invz: invariant zero structure;
- 8) infz: infinite zero structure;
- 9) 1_ invt: left invertibility structure;
- 10) r_invt: right invertibility structure;
- 11) normrank: normal rank;
- 12) v_star: veakly unobservable subspace;
- 13) v_minus: stable weakly unobservable subspace;
- 14) v_plus: unstabl weakly unobservable subspace;
- 15) s_star:strongly controllable subspace;
- 16) s_minus: stable strongly controllable subspace;
- 17) s_plus: unstable weakly unobservable subspace;
- 18) r_ star: strongly controllable weakly unobservable subspace;
 - 19) n_star: distributionally weakly unobservable subspace;
 - 20) s_lambda: geometric subspace S_{λ} ;
 - 21) v_lambda: geometric subspace V_{λ} ;

D) Operations of vector subspaces.

- 1) ssorder: ordering of vector subspaces;
- 2) ssintsec: intersection of vector subspaces;
- 3) ssadd: addition of vector subspaces.

E) Decompositions and properties of descriptor systems.

- 1) ea_ds: decomposition of a matrix pair (E, A);
- 2) sd_ds: decomposition for descriptor systems;
- 3) invz_ds: descriptor system invariant zero structure;
- 4) infz_ds: descriptor system infinite zero structure;
- 5) l_invt_ds: descriptor system left invertibility structure;
- 6) r_invt_ds: descriptor system right invertibility struc-

F) System factorizations.

- 1) mpfact: continuous minimum-phase/all-pass factorization;
 - 2) iofact: continuous-time inner-outer factorization;
 - 3) gcfact: continuous generalized cascade factorization;
- 4) dmpfact: discrete minimum-phase/all-pass factorization:
 - 5) diofact: discrete-time inner-outer factorization.

$\mathbf{G})$ Structural assignment via sensor/actuator selection.

- 1) sa_sen: structural assignment via sensor selection;
- 2) sa_act: structural assignment via actuator selection.

H) Asymptotic time-scale and eigenstructure assignment.

1) atea: continuous-time ATEA;

- 2) gm2star: infimum for continuous-time H2control;
- 3) h2care: solution to continuous-time H2ARE;
- 4) h2state: solution to continuous-time H2control;
- 5) gm8star: infimum for continuous-time H_∞ control;
- 6) h8care: solution to continuous-time H_∞ ARE;
- 7) h8state: solution to continuous-time H_∞ control;
- 8) addps:solution to continuous disturbance decoupling;
- 9) datea: discrete-time ATEA;
- 10) dare: solution to general discrete-time ARE;
- 11) dgm2star: infimum for discrete-time H2 control;
- 12) h2dare: solution to discrete-time H₂ ARE;
- 13) dh2state: solution to discrete-time H₂ control;
- 14) dgm8star: infimum for discrete-time H_∞ control;
- 15) h8dare: solution to discrete-time H_∞ ARE;
- 16) dh8state: solution to discrete-time H_∞ control;
- 17) daddps: solution to discrete-time disturbance decoupling.

Disturbance decoupling with static output feedback.

- 1) ddpcm: solution to disturbance decoupling problem with static output feedback (DDPCM);
- 2) rosys4ddp: irreducible reduced-order system that can be used to solve DDPCM.

3 Descriptions of key m-functions

We briefly describe some key m-functions of the toolkit. In particular, we will present the well-known real Jordan decomposition for autonomous systems, a so-called observability structural decomposition for unforced systems, a block diagonal controllable structural decomposition for unsensed systems, the special coordinate basis, Morse invariance indices and weakly unobservable geometric subspace for proper systems, a structural decomposition technique for singular systems, the inner-outer system factorization, structural assignments through sensor or actuator selection, the asymptotic time-scale eigenstructure assignment, the computation of the best achievable disturbance attenuation level in H_∞ control, and the solution to the problem of disturbance decoupling through static output feedback.

RJD Real Jordan decomposition.

$$[J,T] = RJD(A)$$

generates a transformation that transforms a square matrix into its real Jordan canonical form, i.e.,

$$T^{-1}AT = J = \begin{bmatrix} J_1 & & & \\ & J_2 & & \\ & & \ddots & \\ & & & I_L \end{bmatrix},$$

where each block J_i , $i = 1, 2, \dots, k$, has the following form:

$$J_i = \left[egin{array}{cccc} \lambda_i & 1 & & & \\ & \ddots & \ddots & & \\ & & \lambda_i & 1 & \\ & & & \lambda_i \end{array}
ight]$$

or

$$J_i = \begin{bmatrix} \Lambda_i & I & & & \\ & \ddots & \ddots & & \\ & & \Lambda_i & I & \\ & & & \Lambda_i \end{bmatrix}$$

and λ_i is a real eigenvalue and

$$\Lambda_i = \begin{bmatrix} \mu_i & \omega_i \\ -\omega_i & \mu_i \end{bmatrix}$$

contains a pair of complex eigenvalues $\mu_i \pm j\omega_i$.

OSD Observability structural decomposition.

$$[At, Ct, Ts, To, uom, Oidx] = OSD(A, C)$$

returns an observability structural decomposition for the matrix pair (A, C), i.e.,

$$At = Ts^{-1}ATs = \begin{bmatrix} A_0 & * & 0 & \cdots & * & 0 \\ 0 & * & I_{k_1-1} & \cdots & * & 0 \\ 0 & * & 0 & \cdots & * & 0 \\ \vdots & \vdots & \vdots & & \vdots & \vdots \\ 0 & * & 0 & \cdots & * & I_{k_p-1} \\ 0 & * & 0 & \cdots & * & 0 \end{bmatrix},$$

$$Ct = To^{-1}CTs = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 & 0 \\ \vdots & \vdots & \vdots & & \vdots & \vdots \\ 0 & 0 & 0 & \cdots & 1 & 0 \end{bmatrix},$$

nom: =
$$n - \sum_{i=1}^{r} k_i$$
, Oidx: = $\{k_1, k_2, \dots, k_p\}$.

We note that nom is the number of unobservable modes and the set Oidx is the observability index of (C, A).

BDCSD Block diagonal controllable structural decomposition.

$$[At, Bt, Ts, Ti, ks] = BDCSD(A, B)$$

transforms a controllable pair (A, B) into the block diagonal controllable structureal decomposition form, i.e.,

$$At = Ts^{-1}ATs = \begin{bmatrix} A_1 & 0 & \cdots & 0 \\ 0 & A_2 & \cdots & 0 \\ \vdots & \vdots & & \vdots \\ 0 & 0 & \cdots & A_k \end{bmatrix},$$

$$Bt = Ts^{-1}BT_i = \begin{bmatrix} B_1 & * & \cdots & * & * \\ 0 & B_2 & \cdots & * & * \\ \vdots & \vdots & & \vdots & \vdots \\ 0 & 0 & \cdots & B_k & * \end{bmatrix},$$

$$ks = \{k_1, k_2, \cdots, k_k\},\$$

where A_i and B_i , $i = 1, 2, \dots, k$, are in the form of

$$A_i = \begin{bmatrix} 0 & I_{k_i-1} \\ * & * \end{bmatrix}, B_i = \begin{bmatrix} 0 \\ 1 \end{bmatrix}.$$

SCB Special coordinate basis of continuous-time system.

[
$$As, Bt, Ct, Dt, Gms, Gmo, Gmi, dim$$
]
= $SCB(A, B, C, D)$

decomposes a continuous-time system into the standard SCB form with state subspaces x_a being separated into stable, marginally stable and unstable parts, and x_d being decomposed into chains of integrators.

$$At = \text{Gms}^{-1} A \text{ Gms} = As + B_0 C_0$$

$$= \begin{bmatrix} A_{aa} & L_{ab} C_b & 0 & L_{ad} C_d \\ 0 & A_{bb} & 0 & L_{bd} C_d \\ E_{ca} & L_{cb} C_b & A_{cc} & L_{cd} C_d \\ B_d E_{da} & B_d E_{db} & B_d E_{dc} & A_{dd} \end{bmatrix}$$

$$+ \begin{bmatrix} B_{0a} \\ B_{0b} \\ B_{0c} \\ B_{0c} \end{bmatrix} \begin{bmatrix} C_{0a} & C_{0b} & C_{0c} & C_{0d} \end{bmatrix},$$

$$Bt = Gms^{-1}B Gmi = \begin{bmatrix} B_0 & B_s \end{bmatrix}$$

$$= \begin{bmatrix} B_{0a} & 0 & 0 \\ B_{0b} & 0 & 0 \\ B_{0c} & 0 & B_c \\ B_{0d} & B_d & 0 \end{bmatrix},$$

$$Ct = \text{Gmo}^{-1} C \text{ Gms} = \begin{bmatrix} C_0 \\ C_s \end{bmatrix}$$

$$= \begin{bmatrix} C_{0a} & C_{0b} & C_{0c} & C_{0d} \\ 0 & 0 & 0 & C_d \\ 0 & C_b & 0 & 0 \end{bmatrix},$$

$$Dt = \text{Gmo}^{-1} D \text{ Gmi} = D_s = \begin{bmatrix} I_{m_0} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix},$$

and

$$\dim = [n_a^-, n_a^0, n_a^+, n_b, n_c, n_d],$$

where

$$A_{dd} = A_{dd}^* + B_d E_{dd} + L_{dd} C_d,$$

for some constant matrices $L_{\rm dd}$ and $E_{\rm dd}$ of appropriate dimensions, and

$$\begin{split} &A_{\mathrm{dd}}^{*} = \mathrm{blkdiag}\{A_{q_{1}}, A_{q_{2}}, \cdots, A_{q_{md}}\}\,, \\ &B_{\mathrm{d}} = \mathrm{blkdiag}\{B_{q_{1}}, B_{q_{2}}, \cdots, B_{q_{md}}\}\,, \\ &C_{\mathrm{d}} = \mathrm{blkdiag}\{C_{q_{1}}, C_{q_{2}}, \cdots, C_{q_{-d}}\}\,, \end{split}$$

with $(A_{q_i}, B_{q_i}, C_{q_i})$ being defined as

$$\begin{split} A_{q_i} &= \begin{bmatrix} 0 & I_{q_i-1} \\ 0 & 0 \end{bmatrix}, \\ B_{q_i} &= \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \\ C_{q_i} &= \begin{bmatrix} 1,0,\cdots,0 \end{bmatrix}. \end{split}$$

MORSEIDX Morse invariance indices of proper systems.

$$[11, 12, 13, 14] = MORSEIDX(A, B, C, D)$$

returns Morse structural invariance list:

II = zero dynamics matrix in Jordan form;

I2 = right invertibility structure;

I3 = left invertibility structure;

I4 = infinite zero structure.

V_STAR Weakly unobservable geometric subspace.

$$V = V-STAR(A, B, C, D)$$

computes a matrix whose columns span the geometric subspace V^* .

SD_DS Structural decomposition of continuous-time descriptor system.

$$Gms, Gmo, iGni, dim] = SD_DS(E, A, B, C, D)$$

generates the structural decomposition of a descriptor system. The state x are decomposed as

$$\tilde{x} = \begin{bmatrix} x_z^{\mathsf{T}} & x_e^{\mathsf{T}} & x_a^{\mathsf{T}} & x_b^{\mathsf{T}} & x_c^{\mathsf{T}} & x_d^{\mathsf{T}} \end{bmatrix}^{\mathsf{T}}.$$

The quadruple (Es, As, Bs, Cs, Ds) has the same transfer function as that of the original system. Ez, Psi, Psc, Psd and Psr are some matrices or vectors whose elements are either polynomials or rational functions of s. In particular,

$$\operatorname{Psc} \tilde{x} + \operatorname{Psd} \tilde{u} = \operatorname{Psr} x_z$$
.

See [2] for detail.

IOFACT Inner-outer factorization of continuous-time systems.

[Ai,Bi,Ci,Di,Ao,Bo,Co,Do]
= IOFACT
$$(A,B,C,D)$$

computes an inner-outer factorization for a stable proper transfer function matrix G(s) with a realization (A,B,C,D), in which both $\begin{bmatrix} B^T D^T \end{bmatrix}$ and $\begin{bmatrix} C & D \end{bmatrix}$ are assumed to be of full rank. The inner-outer factorization is given as

$$G(s) = G_i(s) G_o(s),$$

where

$$G_i(s) = \operatorname{Ci}(sI - \operatorname{Ai})^{-1}\operatorname{Bi} + \operatorname{Di}$$

is an inner, and

$$G_{\alpha}(s) = G_{\alpha}(sI - Ao)^{-1}Bo + Do$$

is an outer.

SA_SEN Structural assignment via sensor selection.

$$C = SA_- SEN(A, B)$$

For a given unsensed system (A,B), the function returns a measurement output matrix C such that the

resulting system characterized by (A, B, C) has the pre-specified desired structural properties.

Asymptotic time-scale and eigenstructure as- T =**ATEA** signment.

$$F = ATEA(A, B, C, D[, option])$$

produces a state feedback law u = Fx using the asymptotic time-scale structure and eigenstructure assignment design method for a continuous-time system.

Users have the 'option' to choose the result either in a numerical or in a symbolic form parameterized by a tuning parameter 'epsilon'. The latter is particularly useful in solving control problems, such as H₂ and H_∞ sub-optimal control as well as disturbance decoupling problem.

GM8STAR Infimum or optimal value for continuous

gms8 = GM8STAR
$$(A, B, C, D, E)$$

$$\dot{x} = Ax + Bu + Ew,$$

$$h = Cx + Du,$$

under all possible stabilizing state feedbacks.

DDPCM Disturbance decoupling with static output feedback.

$$K = DDPCM(A, B, E, C1, D1, C2, D2, D22)$$

computes a solution to the disturbance decoupling problem with a constant (static) measurement output feedback forthe following system:

$$\dot{x} = Ax + Bu + Ew,$$

$$y = C1x + D1w,$$

$$h = C2x + D2u + D22w,$$

when the solution exists. Otherwise, the program will return an empty matrix for K.

Numerical examples

In this section, we illustrate a few key m-functions of Linear Systems Toolkit with several numerical examples. Some are straightforward. Others requires reference to the monograph [2] for detailed information.

Example 4.1 (ICF) Consider a Hilbert matrix A given by

$$A = \begin{bmatrix} 1 & 1/2 & 1/3 & 1/4 & 1/5 \\ 1/2 & 1/3 & 1/4 & 1/5 & 1/6 \\ 1/3 & 1/4 & 1/5 & 1/6 & 1/7 \\ 1/4 & 1/5 & 1/6 & 1/7 & 1/8 \\ 1/5 & 1/6 & 1/7 & 1/8 & 1/9 \end{bmatrix}.$$

The m-function [J, T] = JCF(A) returns the Jordan form of A with

$$J = \text{blkdiag} \{3.2879 \times 10^{-6}, 3.0590 \times 10^{-4}, 1.1407 \times 10^{-2}, 2.0853 \times 10^{-1}, 1.5671\},$$

$$T = \begin{bmatrix} -0.0062 & -0.0472 & -0.2142 & 0.6019 & -0.7679 \\ 0.1167 & 0.4327 & 0.7241 & -0.2759 & -0.4458 \\ -0.5062 & -0.6674 & 0.1205 & -0.4249 & -0.3216 \\ 0.7672 & -0.2330 & -0.3096 & -0.4439 & -0.2534 \\ -0.3762 & 0.5576 & -0.5652 & -0.4290 & -0.2098 \end{bmatrix}$$

The computing error is given by

$$||(T^{-1}AT - J)||_2 = 4.0773 \times 10^{-16}.$$

We note that it is hard to obtain a diagonal form for a Hilbert matrix. This example shows that our m-function JCF is capable of handling some rather ill-conditioned matrices.

Example 4.2 (RJD) Consider another constant matrix

GM8STAR Infimum or optimal value for continuous H-infinity control.

gms8 = GM8STAR
$$(A, B, C, D, E)$$

calculates the infimum or the best achievable performance of the H_{∞} suboptimal control problem for the plant,

 $x = Ax + Bu + Ew$,

 $h = Cx + Du$,

$$A = \begin{bmatrix} 3 & 2 & 10 & 0 & 4 & 4 & 4 \\ 2 & 2 & 3 & 1 & 0 & 2 & 1 \\ -1 & 0 & -2 & -1 & 0 & -1 & 0 \\ 2 & 0 & 4 & 4 & -2 & 1 & -2 \\ 3 & 2 & 10 & 2 & 3 & 4 & 2 \\ -1 & -2 & -4 & 0 & -2 & -1 & -2 \\ -3 & -2 & -8 & -1 & -2 & -4 & -2 \end{bmatrix}$$

under all possible stabilizing state feedbacks (1)

The m-function [J, T] = RJD(A) returns a real Jordan form of A with

$$J = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 1 & 1 & 0 \\ 0 & 0 & 0 & -1 & 1 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & -1 & 1 \end{bmatrix}.$$

The transformation matrix T is omitted here.

Example 4.3 (OSD) Consider an unforecd linear system characterized by a matrix pair (A, C) with

$$A = \begin{bmatrix} 0 & 2 & -1 & 1 & 2 & -2 \\ 2 & 8 & 3 & 2 & 9 & 1 \\ -4 & -12 & -6 & -5 & -13 & -2 \\ 2 & 8 & 4 & 3 & 10 & 3 \\ -1 & -6 & -1 & -1 & -7 & 0 \\ 1 & 5 & 1 & 1 & 5 & 0 \end{bmatrix},$$

$$C = \begin{bmatrix} 0 & 1 & 0 & 0 & 1 & 0 \\ 1 & 3 & 1 & 1 & 3 & 0 \end{bmatrix}.$$

The function [At, Ct, Ts, To, uom, Oidx] = osd(A, C)returns the following results:

$$At = \begin{bmatrix} -.1 & -2 & 0 & -2 & 0 & 0 \\ 0 & -1 & 1 & 0 & 0 & 0 \\ 0 & 3 & 0 & -2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 3 & 0 & -4 & 0 & 1 \\ 0 & 5 & 0 & -1 & 0 & 0 \end{bmatrix},$$

and

$$Ct = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix},$$

$$Ts = \begin{bmatrix} 0.50 & -1.50 & -0.50 & 0.75 & -0.75 & 0.75 \\ -0.50 & 0.50 & 0.50 & 0.25 & -0.25 & 0.25 \\ -0.00 & -0.00 & 2.00 & -1.00 & -0.00 & -1.00 \\ -0.50 & -1.50 & -1.50 & 1.25 & 0.75 & 0.25 \\ 0.50 & 0.50 & -0.50 & -0.25 & 0.25 & -0.25 \\ 0.00 & 0.00 & -1.00 & -0.00 & 0.00 & 1.00 \end{bmatrix}$$

$$To = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$
, uom = 1, oidx = $\begin{bmatrix} 2 & 3 \end{bmatrix}$.

There is one unobservable model at -1, and the observability index of (A,C) is given by $\{2,3\}$.

Example 4.4(BDCSD) Consider an unsensed linear system characterized by (A, B) with A as given in (1) and

$$B = \begin{bmatrix} 1 & 0 & 1 & 0 & 1 & 0 & 1 \\ 0 & 1 & 0 & 1 & 0 & 1 & 0 \end{bmatrix}^{\mathrm{T}}.$$

The m-function [At, Bt, Ts, Ti, ks] = BDCSD(A, B)

$$At = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ -4 & 16 & -28 & 28 & -17 & 6 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}, Bt = \begin{bmatrix} 0 & 0.1688 \\ 0 & -0.0998 \\ 0 & -0.0836 \\ 0 & -0.2141 \\ 0 & -0.4276 \\ 1 & 0.0365 \\ 0 & 1.000 \end{bmatrix},$$

$$= \begin{bmatrix} 97.5852 & -211.6782 & 208.9166 & -92.5697 & 15.7616 & 1.0000 & -0.3006 \\ 2.2539 & -15.0155 & 29.3963 & -22.6347 & 5.8731 & 0.1269 & -0.0000 \\ -10.5077 & 33.5232 & -42.7771 & 28.0155 & -9.2539 & 1.0000 & 0.0000 \\ -34.0310 & 61.5542 & -50.7926 & 11.7616 & 1.8731 & 0.1269 & 0.4658 \\ 47.0465 & -107.1085 & 113.6162 & -58.0620 & 13.0155 & 1.0000 & -0.1503 \\ -38.5387 & 77.5852 & -78.0930 & 39.5542 & -10.1424 & 0.1269 & -0.1652 \\ -57.5542 & 140.3778 & -159.8856 & 88.4428 & -21.8886 & 1.0000 & 0.4658 \end{bmatrix}, T_i = \begin{bmatrix} 1.0000 & 0 \\ 0.1269 & 1 \end{bmatrix},$$

and

$$ks = [6 1].$$

Consider a continuous-time proper system characterized by (A, B, C, D) with

$$A = \begin{bmatrix} 1 & 2 & 1 & 4 & 2 \\ -3 & -2 & -1 & -6 & -2 \\ 0 & -1 & 0 & -1 & -1 \\ 4 & 3 & 1 & 7 & 3 \\ -3 & -3 & -1 & -6 & -3 \end{bmatrix}, B = \begin{bmatrix} 0 & 0 \\ -4 & -1 \\ 1 & 0 \\ 3 & 1 \\ -2 & -1 \end{bmatrix}, C = \begin{bmatrix} 3 & 3 & 1 & 7 & 4 \\ 5 & 5 & 2 & 11 & 6 \end{bmatrix}, D = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}.$$

The m-function [As, Bt, Ct, Dt, Gms, Gmo, Gmi, dim] = sub(A, B, C, D) returns the following results:

$$As = \begin{bmatrix} -1.0000 & 0 & 0.1291 & 0 & 0.4518 \\ 0 & 1.0000 & -2.9439 & 0 & -1.4720 \\ 0 & 0 & 0.5000 & 0 & 0.2500 \\ -1.2910 & 1.0190 & -4.5000 & -2 & -4.7500 \\ 1.0328 & -0.9058 & 3.8000 & 2 & 4.5000 \end{bmatrix}, Bt = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 1 \\ 1 & 0 \end{bmatrix}, Ct = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix}, Dt = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, Ct = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix}, Dt = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, Dt = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, Ct = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix}, Dt = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, Dt = \begin{bmatrix} 0$$

and

$$\dim = [1 \ 0 \ 1 \ 1 \ 1].$$

variant zeros at 1 and - 1, respectively, and has a left invertibility index {1}, a right invertibility index {1} and It is straightforward to verify that the system has two in- infinite zero structure {1}. Thus, the system is neither left

nor right invertible.

Using the m-functions V_- STAR and V_- MINUS, we can obtain the weakly unobservable subspace V^+ and stable weakly unobservable subsepace V^- of the given system, which are respectively given by

$$V^* = \begin{bmatrix} 0.0129 & 0.0421 & -0.8608 \\ -0.7000 & 0.3978 & 0.3077 \\ 0.6515 & 0.1578 & 0.3494 \\ 0.0356 & -0.5977 & 0.2037 \\ 0.2902 & 0.6766 & -0.0289 \end{bmatrix},$$

and

$$V^{-} = \begin{bmatrix} 0.0375 & 0.7737 \\ -0.6016 & -0.4879 \\ 0.0000 & 0.0000 \\ 0.5642 & -0.2858 \\ -0.5642 & 0.2858 \end{bmatrix}.$$

5 Conclusion

In the paper, we have presented the contents and descriptions of the software toolbox Linear Systems Toolkit [2]. The package is an effective tool for identifying structural properties of linear systems and it can be used for many applications. We are currently expending the toolkit. More features are being added to the toolkit. Interested readers might access to the most up-to-date information about the toolkit through the website http://linearsystemskit.net or http://hdd.ece.nus.edu.sg/~bmchen.

References

- B. Chen, Z. Lin, Y. Shamash. Linear Systems Theory: A Structural Decomposition Approach [M]. Birkhäuser, Boston, 2004.
- [2] Z. Lin, B. Chen, X. Liv. Linear Systems Toolkit [R] // Technical Report, Department of Electrical and Computer Engineering, University of Virginia, 2004.
- [3] B. Chen. Software Manual for the Special Coordinate Basis of Multivariable Linear Systems [R] // Washington State University Technical Report, No. ECE 0094, Pullman, Washington, 1988.
- [4] Z. Lin. The Implementation of Special Coordinate Basis for Linear Multivariable Systems in MATLAB [R] // Washington State University Technical Report, No. ECE0100, Pullman, Washington, 1989.
- [5] D. Chu, X. Liu, R. C. E. Tan. On the numerical computation of a structural decomposition in systems and control [J]. IEEE Trans. on Automatic Control, 2002, 47(11):1786 1799.
- [6] P. Sannuti, A. Saberi. A special coordinate basis of multivariable linear systems-finite and infinite zero structure, squaring down and decoupling
 [J]. Int. J. of Control., 1987, 45(5):1655 1704.



Xinmin LIU received the bachelor degree of Engineering degree from Beijing Institute of Light Industry in 1989, and master degree of Engineering degrees from Xiamen University and National University of Singapore respectively in 1998 and 2000. He is now pursuing his Ph.D. degree in the Department of Electrical and Computer Engineering at University of Virginia. His current

research interest is in nonlinear systems. Email: xl8y@virginia.edu.



Ben M. CHEN was born in Fuqing, Fujian, China, on November 25, 1963. He received his B. S. degree in mathematics and computer science from Xiamen University, Xiamen, China, in 1983, M. S. degree in electrical engineering from Gonzaga University, Spokane, Washington, USA, in 1988, and PhD degree in electrical & computer engineering from Washington State University,

Pullman, Washington, USA, in 1991.

He was a software engineer in South-China Computer Corporation, Guangzhou, China, from 1983 to 1986. From 1991 to 1992, he was a postdoctoral associate at Washington State University, and was an assistant professor from 1992 to 1993 in the Department of Electrical Engineering, the State University of New York, Stony Brook, New York, USA. Since 1993, he has been with the Department of Electrical and Computer Engineering, the National University of Singapore, where he is currently a professor. His current research interests are in robust control, systems theory, control applications, and development of interner-based laboratories.

Dr Chen has published over 70 internationally refereed journal papers and book chapters, and over 100 articles in international conferences. He is also the author/co-author of 7 monographs, Linear Systems Theory: A Structural Decomposition Approach (Boston: Birkhauser, 2004), Creating Web-Based Laboratories (New York: Springer, 2004), Hard Disk Drive Servo Systems (New York: Springer, 2002), Robust and H_{∞} Control (New York: Springer, 2000), H_{∞} Control and Its Applications (London: Springer, 1998), H_2 Optimal Control (London: Prentice Hall, 1995), and Loop Transfer Recovery: Analysis and Design (London: Springer, 1993).

He was an associate editor for IEEE Transactions on Automatic Control (1999 – 2001), an associate editor for Asian Journal of Control (2002), and a guest co-editor for the Transactions of South African Institute of Electrical Engineers (2002). He is currently serving as an associate editor of the International Journal, Control and Intelligent Systems (2002 –), a member of international advisory board of Kuwait Journal of Science & Engineering (2003 –), an associate editor of Systems & Control Letters (2004 –), and an associate editor of Automatica (2005 –).

Dr Chen was the recipient of the Best Poster Paper Award at the 2nd Asian Control Conference, Seoul, Korea (1997); Asian Young Scholars Award, University of Melbourne, Australia (1997); University Researcher Award, National University of Singapore (2000); Prestigious Engineering Achievement Award, Institution of Engineers, Singapore (2001); Temasek Young Investigator Award, Defense Science & Technology Agency, Singapore (2003); Best Industrial Control Application Prize, 5th Asian Control Conference, Melbourne, Australia (2004). Email: bmchen@nus.edu.sg.



Zongli LIN received his B.S. degree in mathematics and computer science from Xiamen University, Xiamen, China, in 1983, his Master of Engineering degree in automatic control from Chinese Academy of Space Technology, Beijing, China, in 1989, and his Ph.D. degree in electrical and computer engineering from Washington State University, Pullman, Washington, in 1994.

Dr. Lin is currently a professor with the Charles L. Brown Department of Electrical and Computer Engineering at University of Virginia. Previously, he has worked as a control engineer at Chinese Academy of Space Technology and as an assistant professor with the Department of Applied Mathematics and Statistics at State University of New York at Stony Brook.

His current research interests include nonlinear control, robust control, and modeling and control of magnetic bearing systems. In these areas he has published several papers. He is also the author of the book, Low Gain Feedback (Springer-Verlag, London, 1998), a co-author (with Tingshu Hu) of the book Control Systems with Actuator Saturation: Analysis and Design (Birkhauser, Boston, 2001) and a co-author (with B.M. Chen and Y. Sharnash) of the recent book Linear Systems Theory: A Structural Decomposition Approach (Birkhauser, Boston, 2004). For his work on control systems with actuator saturation, he received a US Office of Naval Research Young Investigator Award in 1999.

Dr. Lin served as an Associate Editor of IEEE Transactions on Automatica Control from 2001 to 2003 and is currently an Associate Editor of Automatica and the Corresponding Editor for Conference Activities of IEEE Control Systems Magazine. He is a member of the IEEE Control Systems Society's Technical Committee on Nonlinear Systems and Control and heads its Working Group on Control with Constraints. Email: 215 y@virginia.edu.