

Communication Link Design Problem

Problem Statement

Design a microwave communications link between Gonzaga University and Spokane Community College. Because of obstructions between the two schools, it will be necessary to transmit through a repeater on a tower mountain approximately 7.5 miles from SCC and 8.0 miles from G.U. You are required to consider two designs: 1) one in which a passive repeater is utilized and 2) another in which an active repeater is utilized.

Specifications

Carrier frequencies: $f_c = 6.725$ GHz for 6.675 passive repeater

$$\left. \begin{array}{l} f_{c1} = 6.675 \text{ GHz} \\ f_{c2} = 6.775 \text{ GHz} \end{array} \right\} \text{ for active repeater}$$

Noise bandwidth: 10MHz

SNR at destination: >50dB

Consider only one-way link from G.U. to SCC.

Assumptions

Transmitter power (both at G.U. and repeater): <+20dBm

Receiver Noise Figure (including losses both at SCC and repeater): 8dB

Fading losses (total): <8dB

Antenna Noise Temperature: 290°K

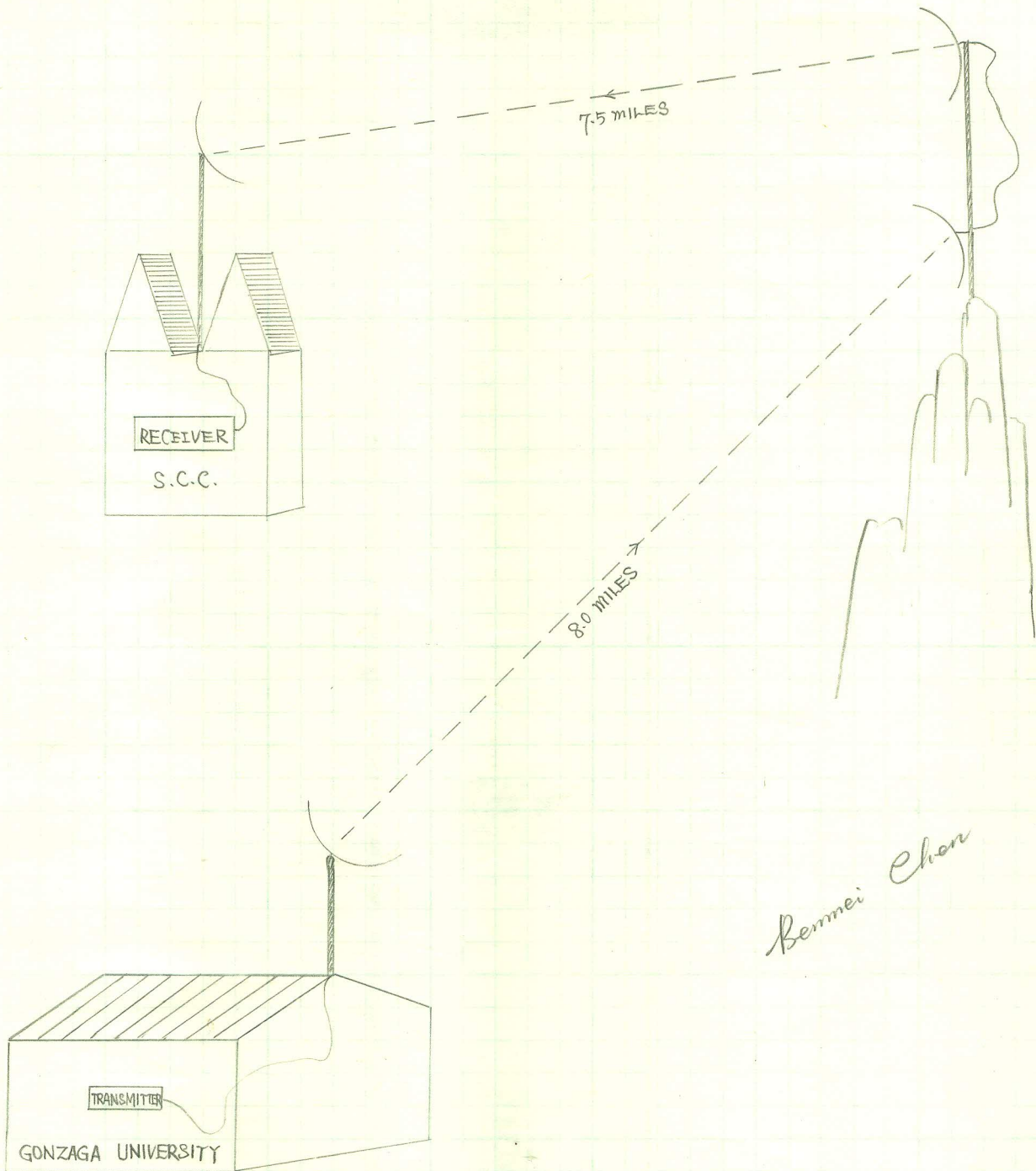
Antenna Efficiency: 55% $G = \frac{2.2\pi A}{\lambda^2}$

Report

The only system components you must specify are antenna sizes and transmitter power levels. Clearly write up your design showing a block diagram with component specifications. You should give signal and noise levels at four points along the link (receiver inputs and transmitter outputs) and mathematically verify that the SNR specification at the destination is satisfied. Discuss the relative advantages and disadvantages of the two designs.

Due Date: December 5, 1986 (no exceptions)

Worth: 100 points toward homework grade.



Communication Link Design Problem.

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November 30, 1986

DESIGN 1 : THE LINK WITH ACTIVE REPEATER

99/100

1. GIVENS AND THE PARAMETERS USED IN DESIGN

$$\text{CARRIER FREQUENCIES} = f_{c1} = 6.675 \text{ GHz}$$

$$f_{c2} = 6.775 \text{ GHz}$$

$$\text{NOISE BANDWIDTH} = 10 \text{ MHz}$$

$$\text{SNR AT DESTINATION} = > 50 \text{ dB}$$

$$\text{TRANSMITTER POWER (BOTH AT G.U. AND REPEATER)} = < +20 \text{ dBm}$$

$$\text{RECEIVER NOISE FIGURE (BOTH AT SCC AND REPEATER)} = F = 8 \text{ dB}$$

$$\text{FADING LOSSES (TOTAL)} = F_L < 8 \text{ dB} = 6.31$$

$$\text{FADING LOSSES FROM G.U. TO REPEATER} = F_{L1} \approx 6.31/2 = 5 \text{ dB}$$

$$\text{FADING LOSSES FROM REPEATER TO SCC} = F_{L2} \approx F_L/2 = 5 \text{ dB}$$

$$\text{ANTENNA NOISE TEMPERATURE} = 290^\circ \text{K}$$

$$\text{ANTENNA EFFICIENCY} = 55\% \quad G = \frac{2.2\pi A}{\lambda^2}$$

$$P_{T1} = \text{TRANSMITTER POWER AT G.U.}$$

$$P_R' = \text{SIGNAL POWER AT THE INPUT OF RECEIVER OF REPEATER.}$$

$$P_{T2} = \text{TRANSMITTER POWER AT REPEATER.}$$

$$P_R = \text{RECEIVED POWER AT S.C.C.}$$

$$\alpha_1 = \text{SIGNAL LOSS FROM G.U. TO REPEATER}$$

$$\alpha_2 = \text{SIGNAL LOSS FROM REPEATER TO S.C.C.}$$

$$d_1 = \text{THE DISTANCE FROM G.U. TO REPEATER} = 8 \text{ miles}$$

$$d_2 = \text{THE DISTANCE FROM REPEATER TO SCC} = 7.5 \text{ miles}$$

$$T_0 = 290^\circ \text{K}$$

$$G_{AR} = \text{THE POWER GAIN OF THE ACTIVE REPEATER.}$$

2. BLOCK DIAGRAM

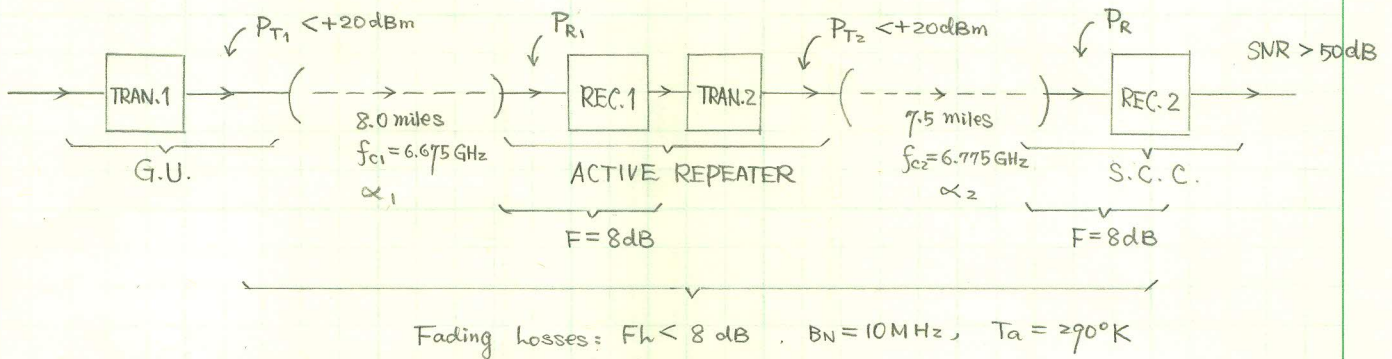


FIG. A1 BLOCK DIAGRAM FOR THE LINK WITH ACTIVE REPEATER

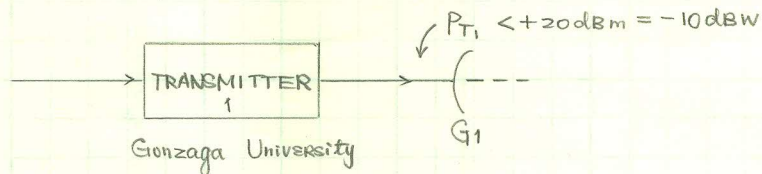


FIG. A2 TRANSMITTER 1 AT G.U.

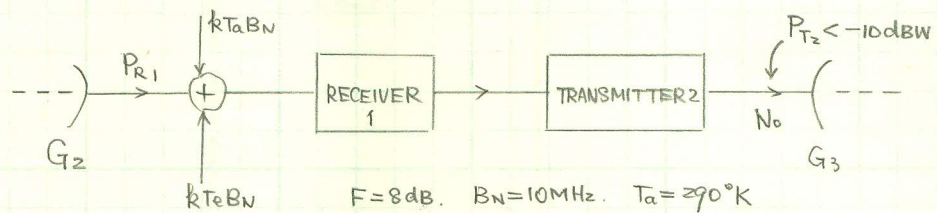


FIG. A3 TRANSMITTER 2 AND RECEIVER 1 (REPEATER)

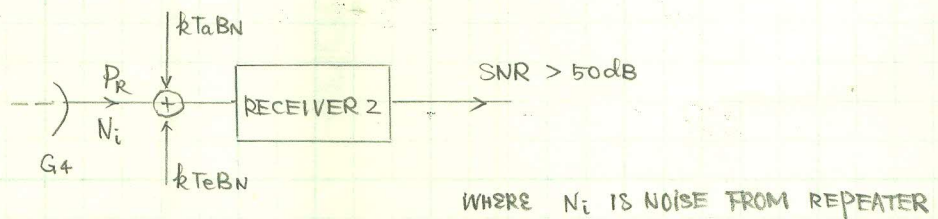
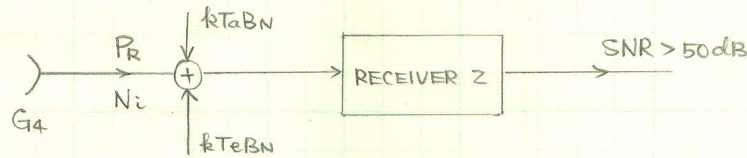


FIG. A4 RECEIVER 2 AT S.C.C.

WHERE N_i IS NOISE FROM REPEATER

3. DESIGN PROCEDURE

a) CONSIDER THE RECEIVER AT S.C.C.: FROM FIG A4 ON PAGE 2 , WE HAVE



$$F = 8 \text{ dB} \quad B_N = 10 \text{ MHz} \quad T_a = 290^\circ \text{ K}$$

$$T_e = (F - 1)T_o = (6.3096 - 1) \times 290^\circ = 1539.7763^\circ \text{ K}$$

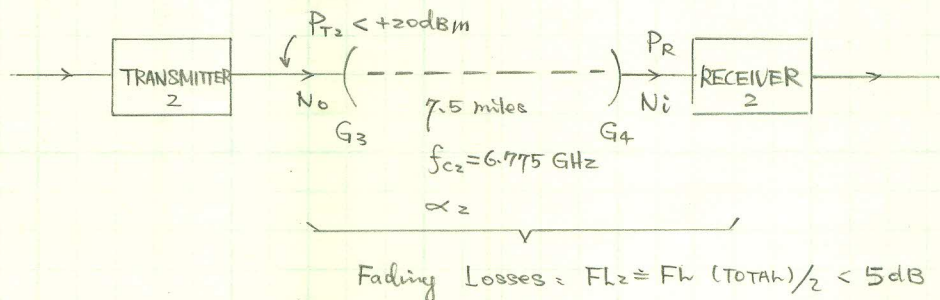
$$\text{SNR} = P_R / (N_i + kT_a B_N + kT_e B_N)$$

$$P_R = \text{SNR} \times (N_i + kT_a B_N + kT_e B_N)$$

$$\geq 10^5 \times (N_i + 1.38 \times 10^{-23} \times 290 \times 10^7 + 1.38 \times 10^{-23} \times 1539.7763 \times 10^7)$$

$$= 2.5251 \times 10^{-8} + 10^5 N_i \quad \text{W} \quad \text{----- (1)}$$

b) CONSIDER THE LINK FROM THE REPEATER TO S.C.C.



$$\alpha_2 = 36.6 + 20 \log_{10} f_{c2} + 20 \log_{10} d_2 \quad (f \text{ in MHz, } d \text{ in miles})$$

$$= 36.6 + 20 \log_{10} 6.775 \times 10^3 + 20 \log_{10} 7.5$$

$$= 130.72 \text{ dB}$$

Because α_2 is greater enough, we can assume $N_i < k(T_a + T_e)B_N = 2.5251 \times 10^{-8} \text{ W}$

$$\text{LET } P_R = 5 \times 10^{-8} \text{ W} = -73.01 \text{ dBW}$$

$$\text{AND } P_{T2} = 19 \text{ dBm} = -11 \text{ dBW} < 20 \text{ dBm}$$

WE CAN ALSO SELECT THE SAME SIZE FOR THE ANTENNA G_3 AND G_4 .

$$P_R = P_{T_2} * G_3 * G_4 / (\alpha_2 * F_{L_2})$$

$$P_R \text{ (dB)} = P_{T_2} \text{ (dB)} + G_3 \text{ (dB)} + G_4 \text{ (dB)} - \alpha_2 \text{ (dB)} - F_{L_2} \text{ (dB)}$$

$$-73.01 \text{ dB} = -11 \text{ dB} + 2G_3 \text{ (dB)} - 130.72 \text{ dB} - 5 \text{ dB}$$

$$G_3 = 36.86 \text{ dB} = 4847.30$$

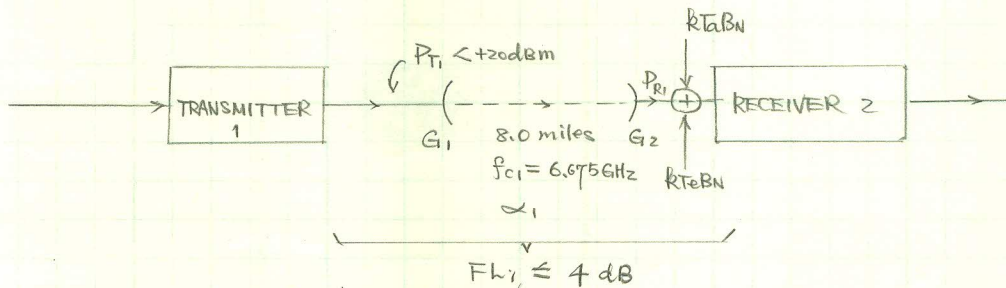
$$G_3 = \frac{2.2\pi A}{\lambda^2} = \frac{2.2\pi A f_{c_2}^2}{c^2}$$

$$A = \frac{G_3 \cdot c^2}{2.2\pi f_{c_2}^2} = \frac{4847.30 \times (3 \times 10^8)^2}{2.2 \times 3.1416 \times (6.775 \times 10^9)^2} = 1.3752 \text{ m}^2$$

$$A = \pi R^2$$

$$R = \sqrt{A/\pi} = \sqrt{1.3752/3.1416} = 0.66 \text{ m}$$

C) CONSIDER THE LINK FROM G.U. TO REPEATER.



WE , NOW , SELECT ANTENNA G_1 AND G_2 WITH DIAMETER = 1.5 m . $\{G \approx G_3\}$

$$G_1 = G_2 = 2.2\pi A f_{c_1}^2 / c^2 = 37.82 \text{ dB}$$

$$\text{LET } P_{T_1} = -11 \text{ dBW} < +20 \text{ dBm}.$$

$$\alpha_1 = 36.6 + 20 \log_{10} f_{c_1} + 20 \log_{10} d_1$$

$$= 36.6 + 20 \log_{10} 6.675 \times 10^3 \text{ MHz} + 20 \log_{10} 8 \text{ miles}$$

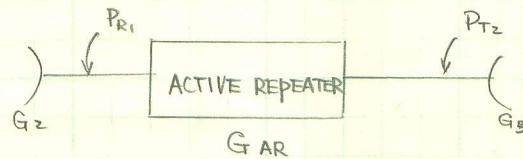
$$= 131.15 \text{ dB}$$

$$F_{L_1} = \frac{1}{2} \times F_L \text{ (TOTAL FADING LOSSES)} = 5 \text{ dB}$$

$$P_{R_1} \text{ (dB)} = P_{T_1} \text{ (dB)} + G_1 \text{ (dB)} - \alpha_1 \text{ (dB)} - F_{L_1} \text{ (dB)} + G_2 \text{ (dB)}$$

$$= -11 \text{ dB} + 37.82 \text{ dB} - 131.15 \text{ dB} - 5 \text{ dB} + 37.82 \text{ dB} = -71.51 \text{ dBW}$$

d) CONSIDER THE POWER GAIN OF REPEATER:



$$P_{R1} = -71.51 \text{ dBW}$$

$$P_{T2} = -11 \text{ dBW}$$

$$G_{AR} = -11 - (-71.51) = 60.51 \text{ dB}$$

4. CONCLUSION:

ANTENNA SIZE = DIAMETER = 1.5 m FOR ONE AT G.U., ONE FOR RECEIVING AT REPEATER

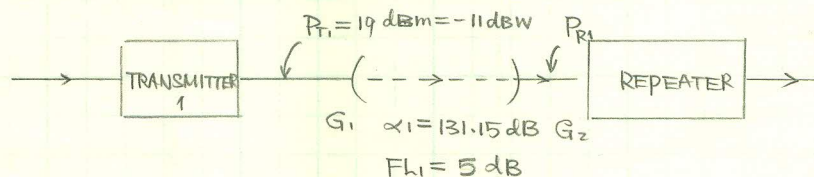
DIAMETER = 1.3 m FOR ONE AT S.C.C, ONE FOR TRANSMITTING AT REPEATER

TRANSMITTER POWER = 19 dBm AT G.U.; REPEATER POWER GAIN = 60 dB

5. VERIFICATION: LOOKING BACK AT THE FIG A1 ON PAGE 2 AND THE COMPONENTS ABOVE,

WE VERIFY THE DESIGN STEP BY STEP AS BELOW.

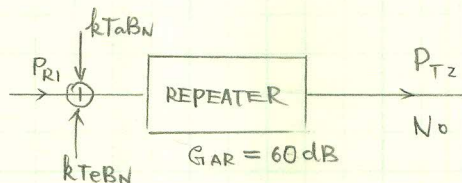
a) FROM G.U. TO REPEATER



$$G_1 = G_2 = \frac{2.2 \times \pi A}{\lambda} = \frac{2.2 \times 3.1416^2 \times 0.75^2 \times 6.675 \times 10^{18}}{9 \times 10^{16}} = 60465 = 37.82 \text{ dB}$$

$$P_{R1} = P_{T1} + G_1 - \alpha_1 - FL_1 + G_2 = -11 + 37.82 - 131.15 - 5 + 37.82 = -71.52 \text{ dBW}$$

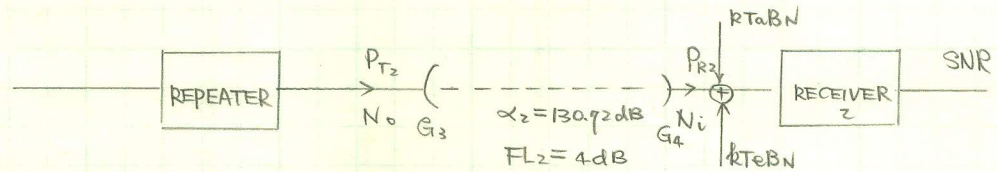
b) REPEATER



$$P_{T2} = P_{R1} + G_{AR} = -71.52 + 60 = -11.52 \text{ dBW} = 18.48 \text{ dBm} < +20 \text{ dBm}$$

$$N_0 = G_{AR} \cdot k(T_a + T_e)B_N = 10^{60} \times 1.23 \times 10^{-23} \times (270 + 1539.78) \times 10^7 = 2.525 \times 10^{-7} = -65.98 \text{ dBm}$$

c) FROM THE REPEATER TO S.C.C.



$$G_3 = G_4 = \frac{2.2 \times \pi^2 \times 0.65^2 \times (6.775 \times 10^9)^2}{9 \times 10^{16}} = 4678.7 = 36.70 \text{ dB}$$

$$N_i = N_0 + G_3 - \alpha_2 - FL_2 + G_4$$

$$= -65.98 + 36.70 - 130.72 - 5 + 36.70 = -128.30 \text{ dB} = 1.48 \times 10^{-13}$$

$$P_{R2} = P_{T2} + G_3 - \alpha_2 - FL_2 + G_4$$

$$= -11.52 + 36.70 - 130.72 - 5 + 36.70 = -73.84 \text{ dB} = 4.1305 \times 10^{-8} \text{ W}$$

$$SNR = P_{R2} / (N_i + k(T_a + T_e)BN)$$

$$= 4.1305 \times 10^{-8} / [1.48 \times 10^{-13} + 1.38 \times 10^{-23} \times 1829.78 \times 10^7]$$

$$= 4.1305 \times 10^{-8} / 4.0051 \times 10^{-13}$$

$$= 103131.0081 = 50.134 \text{ dB} > 50 \text{ dB.} \quad \text{(VERIFIED!)}$$

6. SIGNAL AND NOISE LEVELS AT FOUR POINTS ALONG THE LINK:

POINTS LEVELS (dBm)	G.U. TRANS. OUTPUT	REPEATER REC. INPUT	REPEATER TRANS. OUTPUT	S.C.C. REC. INPUT
SIGNAL	19 dBm	-41.52 dBm	18.48 dBm	-43.84 dBm
NOISE	—	-95.98 dBm	-35.98 dBm	-93.93 dBm

7. IMPROVEMENT

IF WE WANT TO GET SNR MUCH GREATER THAN 50 dB AT DESTINATION WITH THE SAME TRANSMITTER POWER LEVEL, WE MUST INCREASE THE AREAS OF FIRST TWO ANTENNAS AND DECREASE G_{AR} .
eg. CHANGING DIAMETER = 2 m FOR FIRST TWO ANT. AND $G_{AR} = 55 \text{ dB}$, WE HAVE $SNR = 51.40 \text{ dB}$ AT S.C.C.

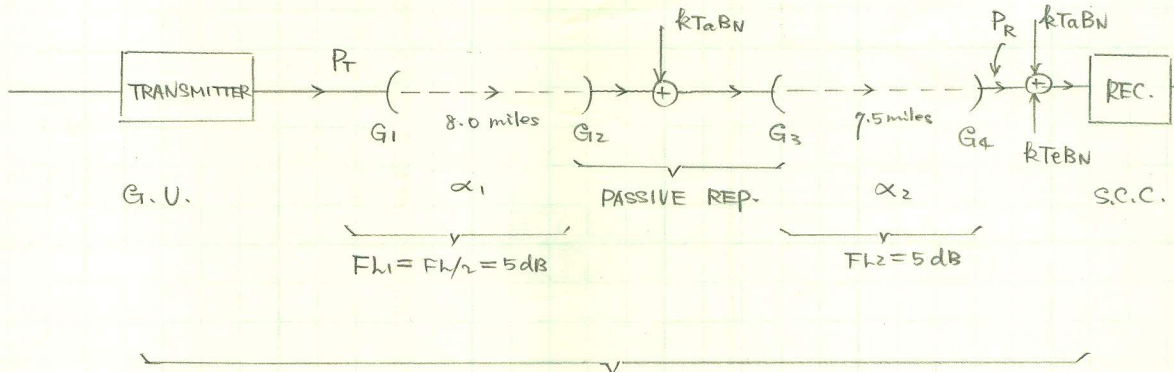
DESIGN 2 = THE LINK WITH PASSIVE REPEATER.

1. GIVENS AND THE PARAMETERS USED IN DESIGN

$$f_{c1} = f_{c2} = f_c = 6.725 \text{ GHz}$$

THE OTHERS ARE THE SAME AS THOSE IN DESIGN 1.

2. BLOCK DIAGRAM



$$f_c = 6.725 \text{ GHz} , B_N = 10 \text{ MHz} , F_L \leq 8 \text{ dB} , T_e = (F - 1) T_o = 1539.77 \text{ } ^\circ \text{K}$$

FIG 1 BLOCK DIAGRAM FOR THE LINK WITH PASSIVE REPEATER

2. DESIGN PROCEDURE:

FROM THE FIG. 1 ON PAGE 7, WE HAVE

$$\begin{aligned} \text{SNR} &= P_R / N \\ &= P_R / [N_i + k(T_a + (F-1)T_0)B_N] \quad \dots (1) \end{aligned}$$

WHERE, $T_a = 290^\circ\text{K}$, $T_0 = 290^\circ\text{K}$, $F = 8\text{dB} = 6.31$, $B_N = 10\text{MHz}$

$$N_i = N_0 * G_3 * G_4 / \alpha_2 \cdot FL_2, \quad N_0 = kT_a B_N$$

$$P_R = P_T * G_1 * G_2 * G_3 * G_4 / (\alpha_1 * \alpha_2 * FL)$$

LET US SELECT THE SAME SIZE FOR ALL THE FOUR ANTENNA, SO,

$$G_1 = G_2 = G_3 = G_4 = G$$

REWRITE THE EQUATION (1), WE HAVE

$$\text{SNR} = P_T \times G^4 / \{(\alpha_1 \alpha_2 \cdot FL) * [k B_N (G^2 \cdot T_a / \alpha_2 \cdot FL_2 + F \cdot T_0)]\} \quad \dots (2)$$

$$\alpha_1 = 36.6 + 20 \log_{10} f_c + 20 \log_{10} d_1 \quad (f_c \text{ IN MHz, } d_1 \text{ IN MILES})$$

$$= 36.6 + 20 \log_{10} 6.725 \times 10^3 + 20 \log_{10} 8 = 131.22 \text{ dB}$$

$$= 1.323 \times 10^{13}$$

$$\alpha_2 = 36.6 + 20 \log_{10} f_c + 20 \log_{10} d_2$$

$$= 36.6 + 20 \log_{10} 6.725 \times 10^3 + 20 \log_{10} 7.5$$

$$= 130.66 \text{ dB} = 1.1628 \times 10^{13}$$

$$FL = 8\text{dB} = 10^{.8} = 6.31$$

$$FL_2 = 5\text{dB} = 3.1623$$

$$F = 8\text{dB} = 10^{.8} = 6.31$$

$$\text{LET } \text{SNR} = 50\text{dB} = 10^5$$

$$\text{LET } P_T \cong 19\text{dBm} = -11\text{dBW} = 0.0794$$

NOW, REWRITE EQUATION (2), WE GET

$$G^4 - 1331553.73 G^2 + 3.0873 \times 10^{20} = 0$$

$$G = 132557.0823 = 51.22 \text{ dB}$$

$$G = \frac{2.2\pi A}{\lambda^2}$$

$$A = \frac{G \times c^2}{2.2\pi \times f_c^2} = \frac{132551.4118 \times (3 \times 10^8)^2}{2.2 \times 3.1416 \times (6.675 \times 10^9)^2} = 38.74 \text{ m}^2$$

$$R = \sqrt{A/\pi} = \sqrt{38.74/3.1416} = 3.5 \text{ m}$$

3. CONCLUSION :

ANTENNA SIZE : DIAMETER = 7m FOR ALL FOUR ANTENNA.

TRANSMITTER POWER : 19.5 dBm AT G.U.

4. VERIFICATION :

$$G = G_1 = G_2 = G_3 = G_4 = 51.22 \text{ dB}$$

$$P_t = 19.5 \text{ dBm} = -10.5 \text{ dBW}$$

$$\alpha_1 = 131.22 \text{ dB}$$

$$\alpha_2 = 130.66 \text{ dB}, \quad F_L = 8 \text{ dB}$$

$$P_R = P_t + G_1 - \alpha_1 + G_2 + G_3 - \alpha_2 + G_4 - F_L \quad (\text{IN dB})$$

$$= -10.5 + 51.22 - 131.22 + 51.22 + 51.22 - 130.66 + 51.22 - 8$$

$$= -75.5 \text{ dBW}$$

$$N_o = k T_a B_N = 1.38 \times 10^{-23} \times 290 \times 10^7 = -133.98 \text{ dB}$$

$$N_i = N_o + G_3 - \alpha_2 - F_{L2} + G_4$$

$$= -133.98 + 51.22 - 130.66 - 5 + 51.22 = -167.20 \text{ dBW} = 1.91 \times 10^{-17} \text{ W}$$

$$N = N_i + k[(F-1)T_o + T_a]B_N$$

$$= 1.9 \times 10^{-17} + 1.38 \times 10^{-23} \times 1829.776 \times 10^7$$

$$= 2.525 \times 10^{-13} \text{ W} = -125.98 \text{ dB}$$

$$\text{SNR} = P_R - N \quad (\text{IN dB})$$

$$= -75.5 - (-125.98)$$

$$= 50.48 \text{ dB} > 50 \text{ dB.} \quad \underline{\underline{(\text{VERIFIED !!})}}$$

5. SIGNAL AND NOISE LEVELS AT THE TRNS. OUTPUT AND REC. INPUT :

$$P_T = 19.5 \text{ dBm} ; \quad P_R = -45.5 \text{ dBm} , \quad N_{IR} = -95.98 \text{ dBm}$$

COMPARE :

FROM THE DESIGNS WE GOT , WE ARE EASY TO FIND OUT THAT: IN DESIGN 1 ,
THE LINK WITH ACTIVE REPEATER , WE ONLY NEED TO USE 1.5m-DIAMETER ANTENNAS
FOR TRANSMITTING AT G.U. AND RECEIVING AT THE REPEATER , AND 1.3m-DIAMETER
ANTENNAS FOR TRANSMITTING AT THE REPEATER AND RECEIVING AT S.C.C., HOWEVER ,
WE NEED TO EMPLOY A 60dB-POWER-GAIN REPEATER .

IN DESIGN 2 , WE DON'T NEED TO USE A ACTIVE REPEATER WITH RECEIVER
AND TRANSMITTER. BUT , WE MUST USE FOUR 7m-DIAMETER ANTENNAS IN THE
LINK .

IT SEEMS THAT DESIGN 1 IS MORE REASONABLE THAN DESIGN 2 .